



Metropolitan Water Reclamation District of Greater Chicago
Protecting Our Water Environment

**Feasibility of Traditional and Emerging Technologies
for Treatment and Resource Recovery from Recycle
Streams at the Water Reclamation Plants of
Metropolitan Water Reclamation District of Greater
Chicago**

Presented by

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November 19, 2010

Acknowledgement

1. M&O staff are acknowledged for their assistance to help identify recycle streams, recycle flow lines and the safe sampling locations:
 - Peter Kane, and Mark Kwan at SWRP
 - Raphael Frost, Paul Wysocki, Greg Florek, & Roberto Sanchez at CWRP
 - Mary Brand and Katryzyna Lai at EWRP
2. Shop trade personnel at SWRP fabricated a lab-scale five-branch manifold for expedient filtration of samples
3. IWD Staff set-up and serviced auto samplers & collected and transported samples:
 - Renaud Robert; Turner, David; Yore Michael; Yarnik, Greg; McCune, Michael; Gaggiano, Roberet; Chodora James; Spiewak, Steven; Gardner, Edward; Waclawick, James (Retired); Geraghty, Thomas; Ms. Rogers, Marshalyn and their staff
4. Harold Robinson, Wastewater Tech
5. ALD Staff at CAL, EAL and SAL for analytical support:
 - Victor Olchowka, Ellice Durham, Robert Polis, Joseph Calvano, Gary Pump, John Chavich and their staff
6. Dori Bernstein, Research Scientist for GPS-X Modeling support
7. Pro-Corp, LLC and Ostara Inc. for screening recycle streams and analyzing data for cost opinions

OUTLINE

- **Identification of Recycle Streams at Stickney, Calumet and Egan WRPs**
- **Sampling Locations - Raw Sewage and Recycle Streams**
- **Sampling Plan**
- **Estimation of Flow and Characteristics Data of Recycle Streams**
- **Loadings at Plant Headworks**
- **Impact on Treatment at SWRP**
- **Treatment Options and Screening of Technologies**
- **Feasible Technologies for District WRPs**

Identification of Recycle Streams at Calumet, Egan and Stickney WRPs



Centrate

East side lagoon 9 supernatant overflow plus runoff from drying cells
West side lagoon 17 supernatant overflow,
Gravity tank supernatant overflow
(Digester feed tank overflow and Gravity concentration feed tank overflow seldom)



Centrate

GBT filtrate
Grit Classifier Recycle
Filter Backwash

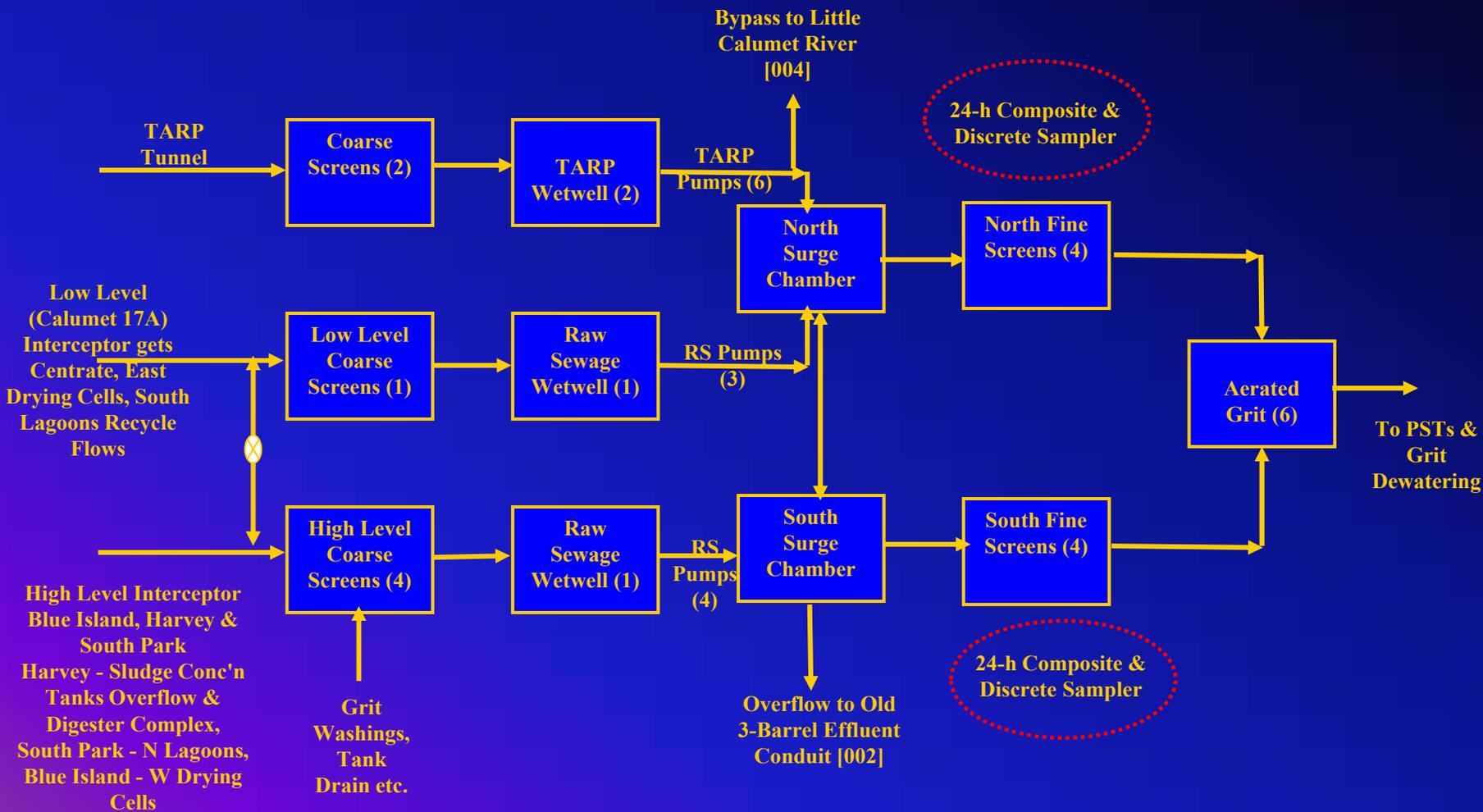


Pre-centrifuge centrate

Post-centrifuge centrate

Gravity Concentration tank supernatant overflow
(Lagoon supernatant via main screen seldom)

Details of Plant Headworks and Recycle Streams at Calumet WRP



CENTRATE



GRAVITY OVERFLOW



LAGOON 9



SAMPLING LOCATIONS AT CALUMET WRP

LAGOON 17



LAGOON 17



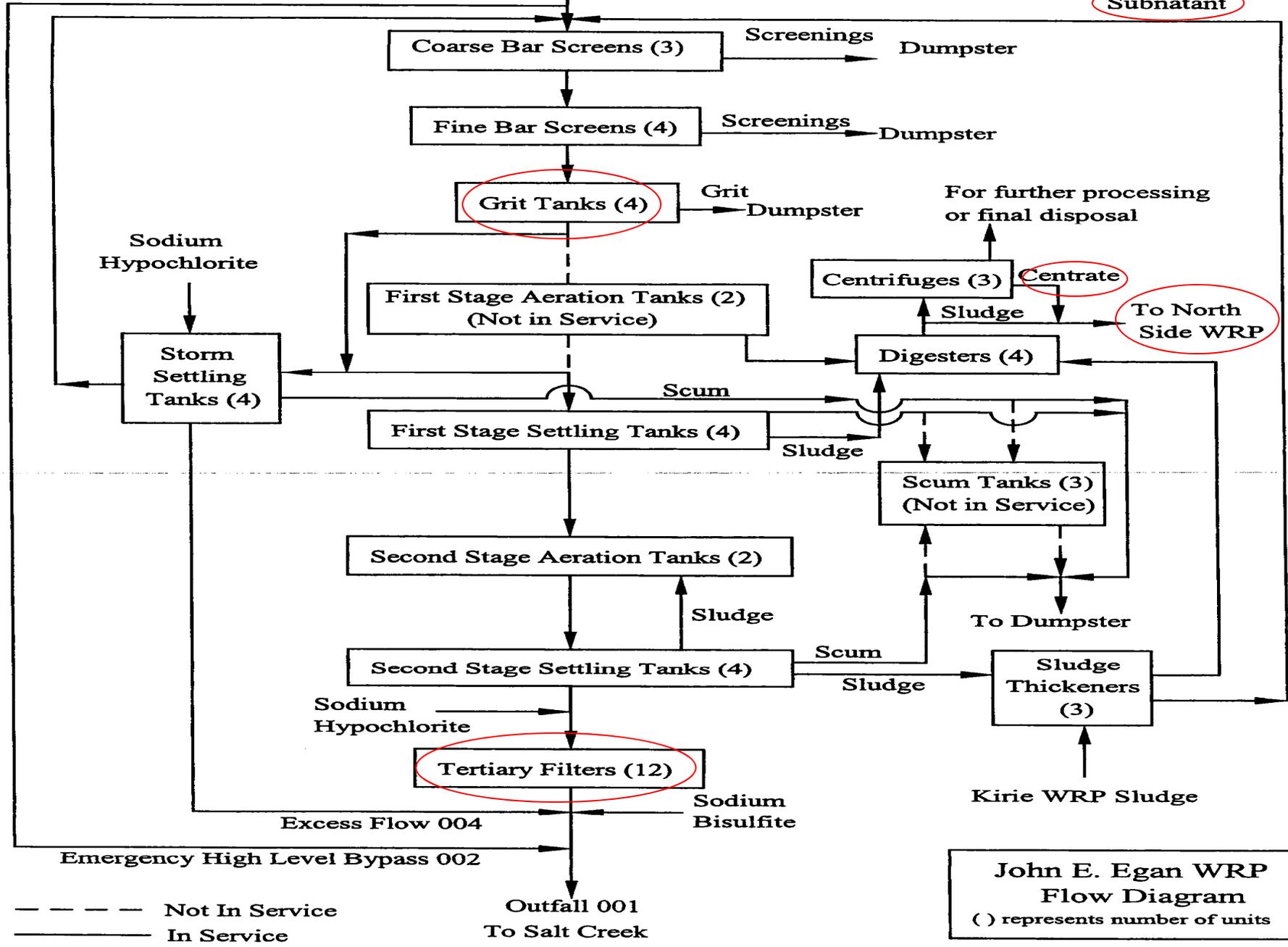
LAGOON 9



Upper Salt Creek No. 1

Upper Salt Creek No. 10

Subnatant



**John E. Egan WRP
Flow Diagram**
() represents number of units

--- Not In Service
— In Service



Grit Classifier

SAMPLING LOCATIONS AT EGAN WRP



GBT Filtrate

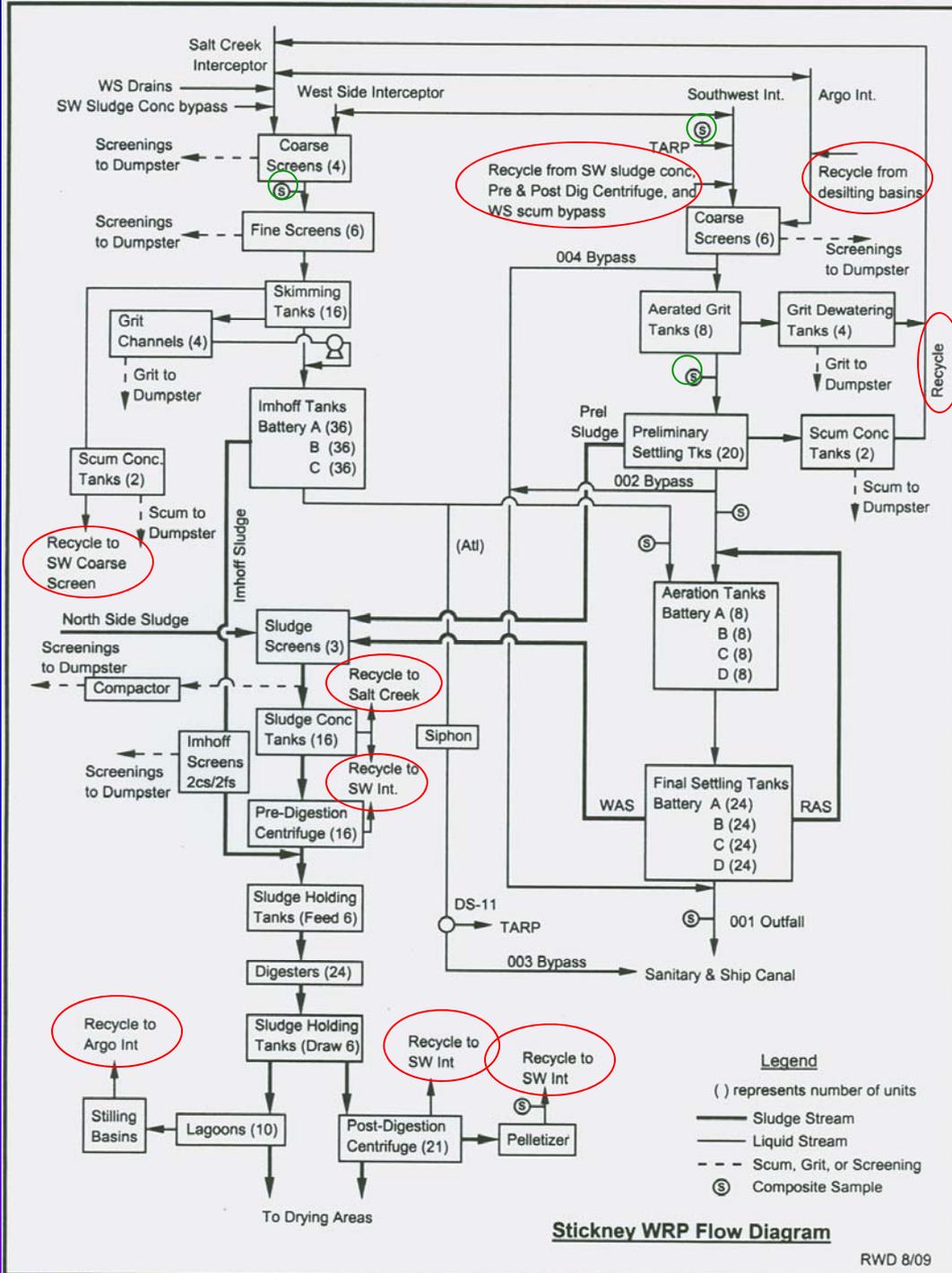


Centrate



Filter Backwash

STICKNEY WRP



Stickney WRP Flow Diagram

SAMPLING LOCATIONS AT STICKNEY WRP



SAMPLING LOCATIONS AT PRE AND POST-CENTRIFUGE FACILITIES AT STICKNEY WRP





SPOCTC1 OLD POST CENTRIFIUGES



SCTC COMPOSITE CENTRATE



NOTICE
This area contains hydrogen sulfide gas.
Hydrogen sulfide gas is highly toxic and flammable.
Do not enter this area without proper training and equipment.

HYDROGEN SULFIDE
GAS ALARM

CONCENTRATION
BUILDING
BUILDING NO. 102

CAUTION
HOT WORK PERMIT
REQUIRED IN
THIS AREA

WARNING

HAVE PORTABLE GAS
DETECTION EQUIPMENT
WITH YOU WHEN
FIXED SYSTEM
IS NOT WORKING

FIRE
HYDRANT
VALVE
SIDE

5

Inde
Recy
Serv
312

SAMPLING PLAN

- TIME COMPOSITES COLLECTED EVERY 15-MINUTE APART OVER 24-HOUR PERIOD TO MAKE APPROXIMATELY 2 GALLONS AT EACH STATION**
- STICKNEY AND CALUMET WRP - ONCE A WEEK (7/30/08-7/29/09)**
- EGAN WRP - TWICE A WEEK (8/11/09-9/3/09)**

CHARACTERISTICS OF RECYCLE STREAMS AND RAW SEWAGE AT CALUMET WRP (7/30/08-7/29/09)

| Parameter | Raw Sewage | Centrate | Gravity Supernatant | Lagoon 9 (East) | Lagoon 17 (West) | Combined Recycle |
|--------------------------|------------|----------|---------------------|-----------------|------------------|------------------|
| Flow, MGD | 307 | 0.6 | 4.0 | 0.45 | 0.45 | 5.5 |
| BOD ₅ , mg/L | 113 | 139 | 158 | 50 | 118 | 143 |
| SS, mg/L | 148 | 768 | 493 | 99 | 653 | 504 |
| NH ₃ -N, mg/L | 10 | 286 | 7 | 80 | 308 | 68 |
| TKN, mg/L | 21 | 495 | 33 | 128 | 487 | 128 |
| Tot P, mg/L | 5 | 32 | 17 | 11 | 53 | 21 |

CHARACTERISTICS OF RECYCLE STREAMS AND RAW SEWAGE AT EGAN WRP (8/11/09-9/3/09)

| Parameter | Raw Sewage | Centrate | Filter Backwash | GBT Filtrate | Grit Classifier | Combined Recycle |
|--------------------------|------------|----------|-----------------|--------------|-----------------|------------------|
| Flow, MGD | 24 | 0.25 | 1.8 | 1 | 0.12 | 3.17 |
| BOD ₅ , mg/L | 267 | 80 | 13 | 393 | 265 | 148 |
| SS, mg/L | 344 | 695 | 59 | 998 | 286 | 414 |
| NH ₃ -N, mg/L | 17 | 277 | 2 | 4 | 17 | 25 |
| TKN, mg/L | 37 | 289 | 7 | 58 | 35 | 46 |
| Tot P, mg/L | 9 | 23 | 5 | 32 | 9 | 15 |

1. Centrate is pumped to Northside WRP
2. Combined recycle concentrations include centrate input

CHARACTERISTICS OF RECYCLE STREAMS AND RAW SEWAGE AT STICKNEY WRP (7/30/08-7/29/09)

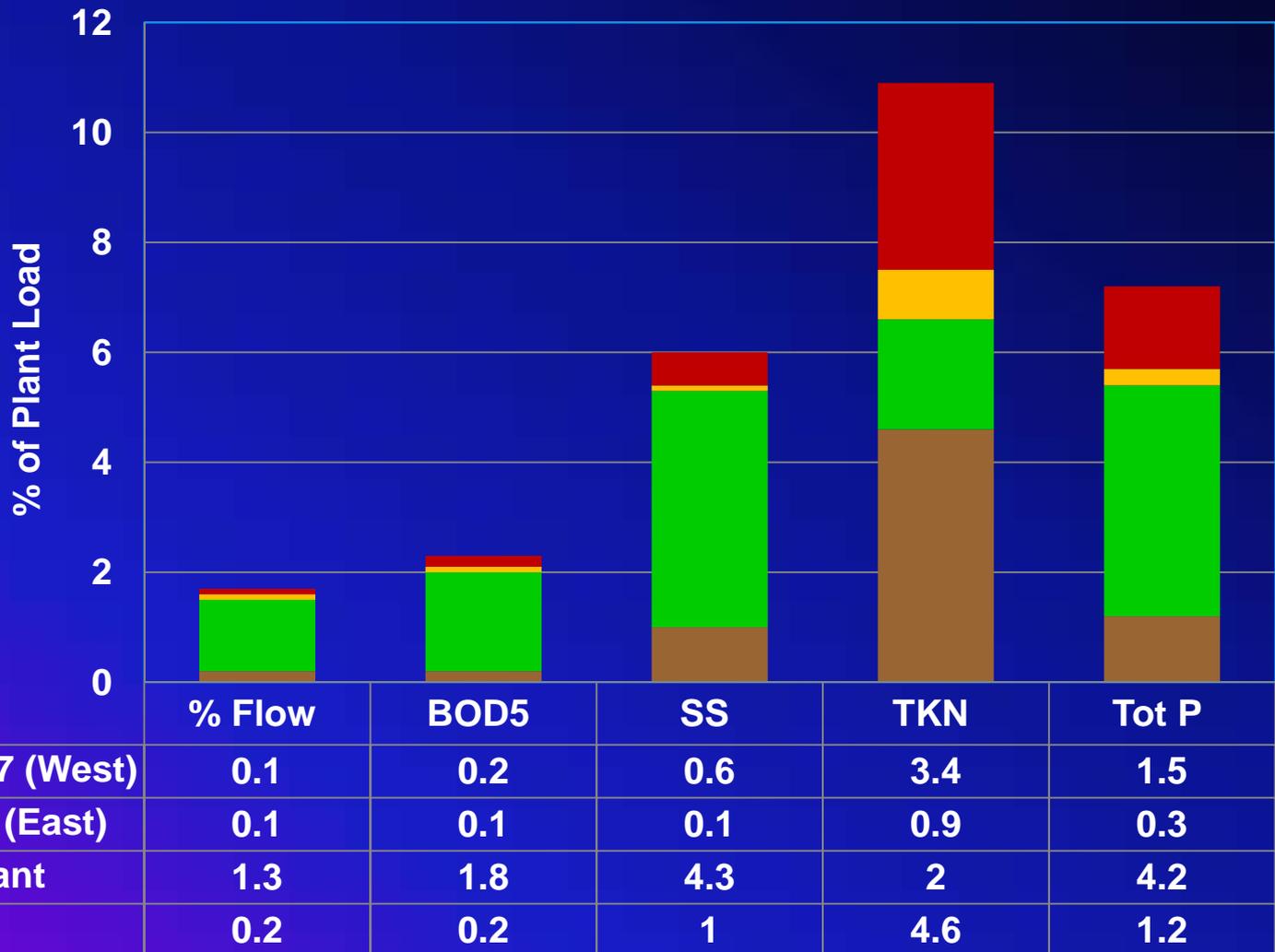
| Parameter, MGD or mg/L | Raw Sewage SW+WS | Post centrifuge centrate New | Post centrifuge centrate Old | Pre- centrifuge centrate | Centrate composite | Gravity Concentr- ation Tanks Overflow | Combined Recycle |
|------------------------------|------------------------|---------------------------------------|---------------------------------------|--------------------------------|-----------------------|--|---------------------|
| Flow | 804 | 1.4 | 1.4 | 10.9 | 13.7 | 13 | 26.7 |
| BOD ₅ | 192 | 79 | 127 | 853 | 1,085 | 371 | 677 |
| SS | 322 | 336 | 452 | 929 | 1,307 | 731 | 978 |
| NH ₃ -N | 15 | 291 | 481 | 20 | 174 | 15 | 83 |
| TKN | 30 | 332 | 564 | 120 | 266 | 65 | 151 |
| Tot P | 6 | 36 | 54 | 45 | 56 | 23 | 37 |

COMPARISON OF FLOW AND CHARACTERISTICS OF CENTRATE STREAMS AT VARIOUS PLANTS

| WWTP | Flow, m ³ /d | Centrt Flow, m ³ /d | % | NH ₄ -N, mg/L | sCOD | TP, mg Per L | pH | Alkalinity, mg/L as CaCO ₃ | sCOD/NH ₄ | Authors |
|-----------------------|-------------------------|--------------------------------|------|--------------------------|-------|--------------|-----|---------------------------------------|----------------------|-------------------------|
| Wards Island, NY, USA | 937,500 | 19,125 | 2.04 | 886 | 431 | 79 | 7.7 | 2,943 | 0.50 | Katehis et al. (1998) |
| Hunts Point, NY, USA | 750,000 | 14,250 | 1.9 | 1,312 | 793 | 112 | 7.9 | 5,265 | 0.60 | Katehis et al. (1998) |
| 26th Ward, NY, USA | 318,750 | 7,125 | 2.2 | 801 | 494 | 84 | 7.8 | 3,144 | 0.62 | Katehis et al. (1998) |
| Bowery Bay, NY, USA | 562,500 | 5,250 | 0.9 | 672 | 371 | 116 | 7.5 | 2,100 | 0.55 | Katehis et al. (1998) |
| Kohlfurth, Germany | 103,680 | 300 | 0.3 | 628 | 1,760 | - | - | - | 2.8 | Kolish and Rolfs (2000) |
| Calumet WRP | 1,160,460 | 2,268 | 0.2 | 286 | 260 | 32 | 7.9 | 1,529 | 0.91 | Patel (2010) |
| Egan WRP | 91,098 | 945 | 1 | 277 | 201 | 17 | 7.6 | 228 | 0.73 | Patel (2010) |
| Stickney WRP | 3,039,120 | 10,433 | 0.3 | 386 | 300 | 11 | 7.9 | 494 | 0.78 | Patel (2010) |

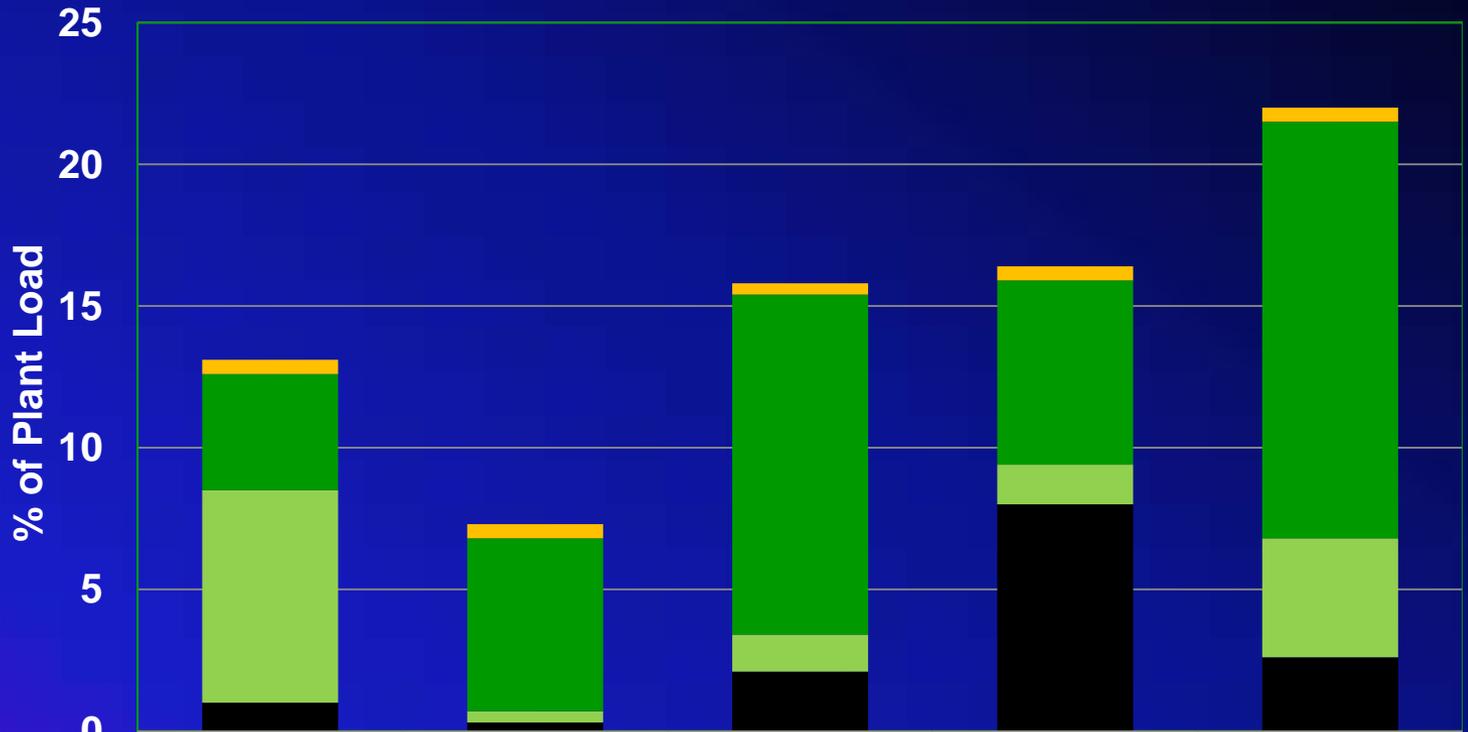
RECYCLE CONTRIBUTION TO INFLUENT FLOW AT CALUMET WRP (7/30/08-7/29/09)

| | |
|---------------------|---------|
| Flow, MGD | 307 |
| BOD ₅ | 289,323 |
| SS | 378,936 |
| TKN | 53,768 |
| Tot P | 13,314 |
| Loadings in lbs/day | |



RECYCLE CONTRIBUTION TO INFLUENT FLOW AT EGAN WRP (8/11/09-9/3/09)

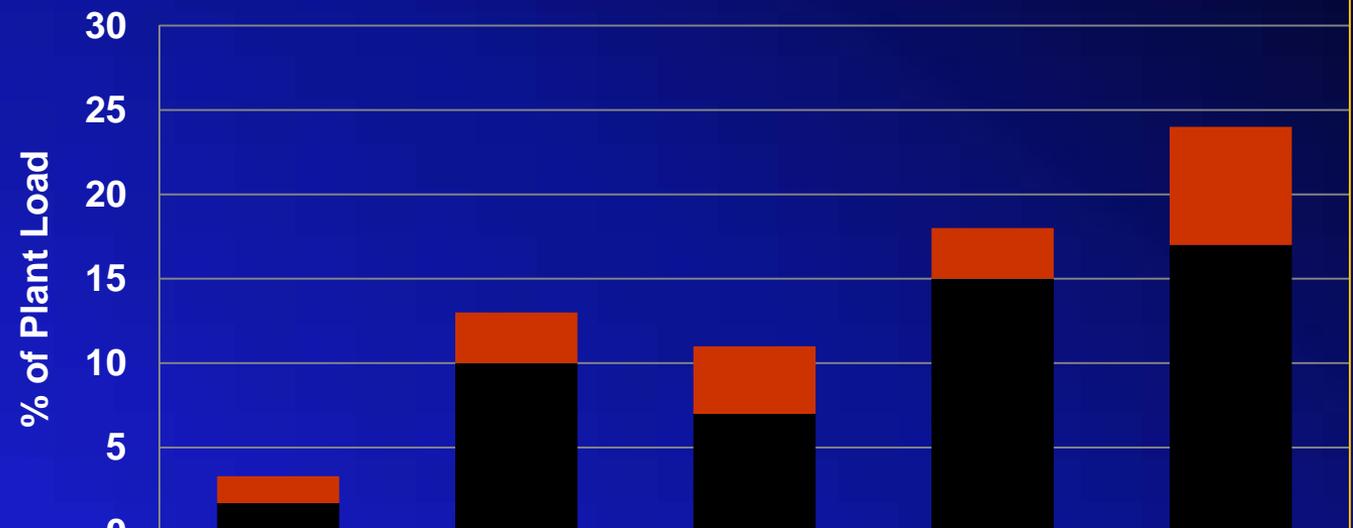
| | |
|---------------------|--------|
| Flow, MGD | 24.1 |
| BOD ₅ | 53,573 |
| SS | 69,142 |
| TKN | 7,477 |
| Tot P | 1,809 |
| Loadings in lbs/day | |



| | % Flow | BOD5 | SS | TKN | Tot P |
|---------------------------|--------|------|-----|-----|-------|
| ■ Grit Classifier Recycle | 0.5 | 0.5 | 0.4 | 0.5 | 0.5 |
| ■ GBT Filtrate | 4.1 | 6.1 | 12 | 6.5 | 14.7 |
| ■ Filter Backwash | 7.5 | 0.4 | 1.3 | 1.4 | 4.2 |
| ■ Centrate | 1 | 0.3 | 2.1 | 8 | 2.6 |

RECYCLE CONTRIBUTION TO INFLUENT FLOW AT STICKNEY WRP (7/30/08-7/29/09)

| | |
|---------------------|-----------|
| Flow, MGD | 804 |
| BOD ₅ | 1,289,469 |
| SS | 2,157,382 |
| TKN | 202,401 |
| Tot P | 36,861 |
| Loadings in lbs/day | |



| | % Flow | BOD5 | SS | TKN | Tot P |
|--|--------|------|----|-----|-------|
| ■ Gravity Concentration Tanks Overflow | 1.6 | 3 | 4 | 3 | 7 |
| ■ Centrate composite | 1.7 | 10 | 7 | 15 | 17 |

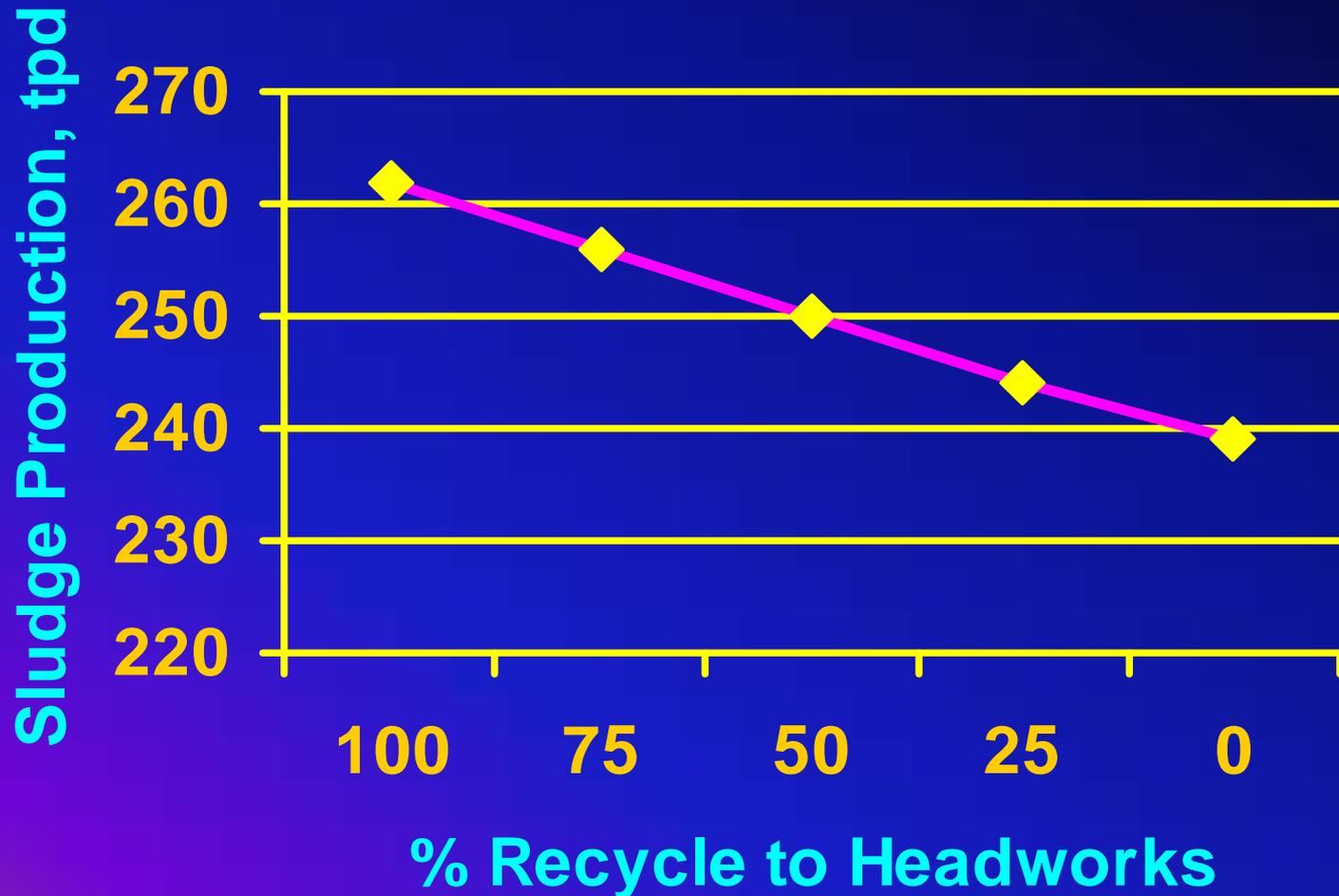
STICKNEY WRP GPS-X MODEL

- **Black & Veach 2000 GPS-X – No recycle lines**
- **Modifications – recycle lines to headworks or final outfall via sidestream treatment unit**
- **Baseline data correspond to study period with plant and LIMS data and calibrated throughout the process train based on 100% recycle to headworks**
- **Added a DO controller to evaluate potential energy savings due to aeration**
- **Each scenario consisted of three 100-day simulations to assure stability**

STICKNEY GPS-X BASELINE MODEL: 100% RECYCLE TO HEADWORKS

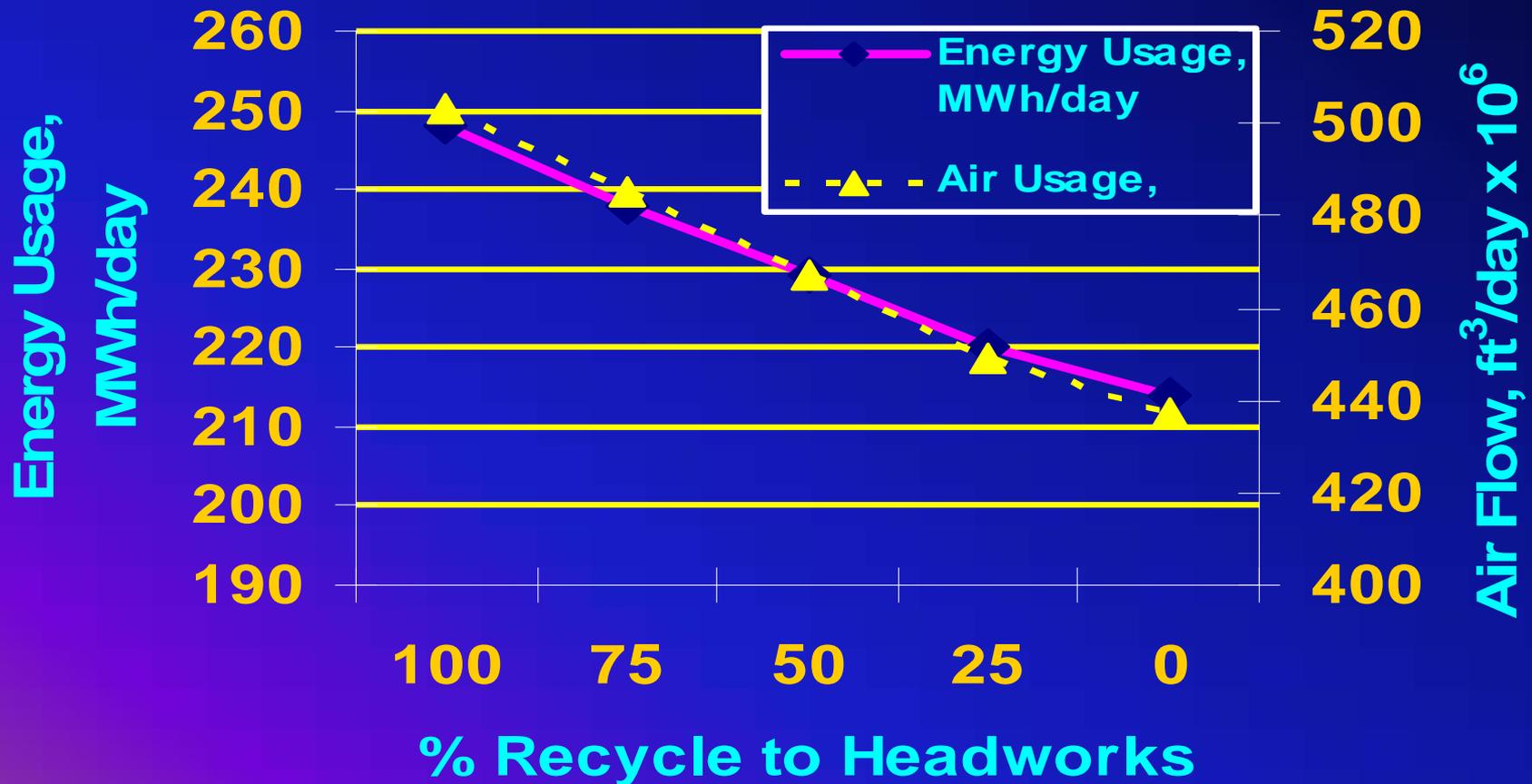
| Parameter | WS Influent | SW Influent + TARP | All Recycle | Final Effluent |
|-------------------------------------|-------------|--------------------|-------------|----------------|
| Flow, MGD | 431 | 340 | 26 | 772 |
| SS, mg/L (tpd) | 150 (270) | 530 (809) | 988 (108) | 4.8 (15.5) |
| CBOD₅, mg/l (tpd) | 77 (139) | 169 (258) | 332 (36) | 1.5 (4.9) |
| TKN, mg/L (tpd) | 19 (34) | 47 (71) | 156 (17) | 0.9 (3.0) |
| TP, mg/L (tpd) | 4 (6) | 9 (14) | 37 (4) | 0.8 (1.2) |
| NH₃-N, mg/L (tpd) | 10 (18) | 19 (29) | 94 (10) | 0.1 (0.2) |

Stickney GPS-X Model: Sludge Production as a Function of Percent Recycle to Headworks



Stickney GPS-X Model: Air and Energy Usage as a Function of Percent Recycle to Headworks

Normal plant operation : 496×10^6 cft/day & aeration energy 368 MWH/day
DO control set point of 4.5 mg/L. Results in ~15% savings

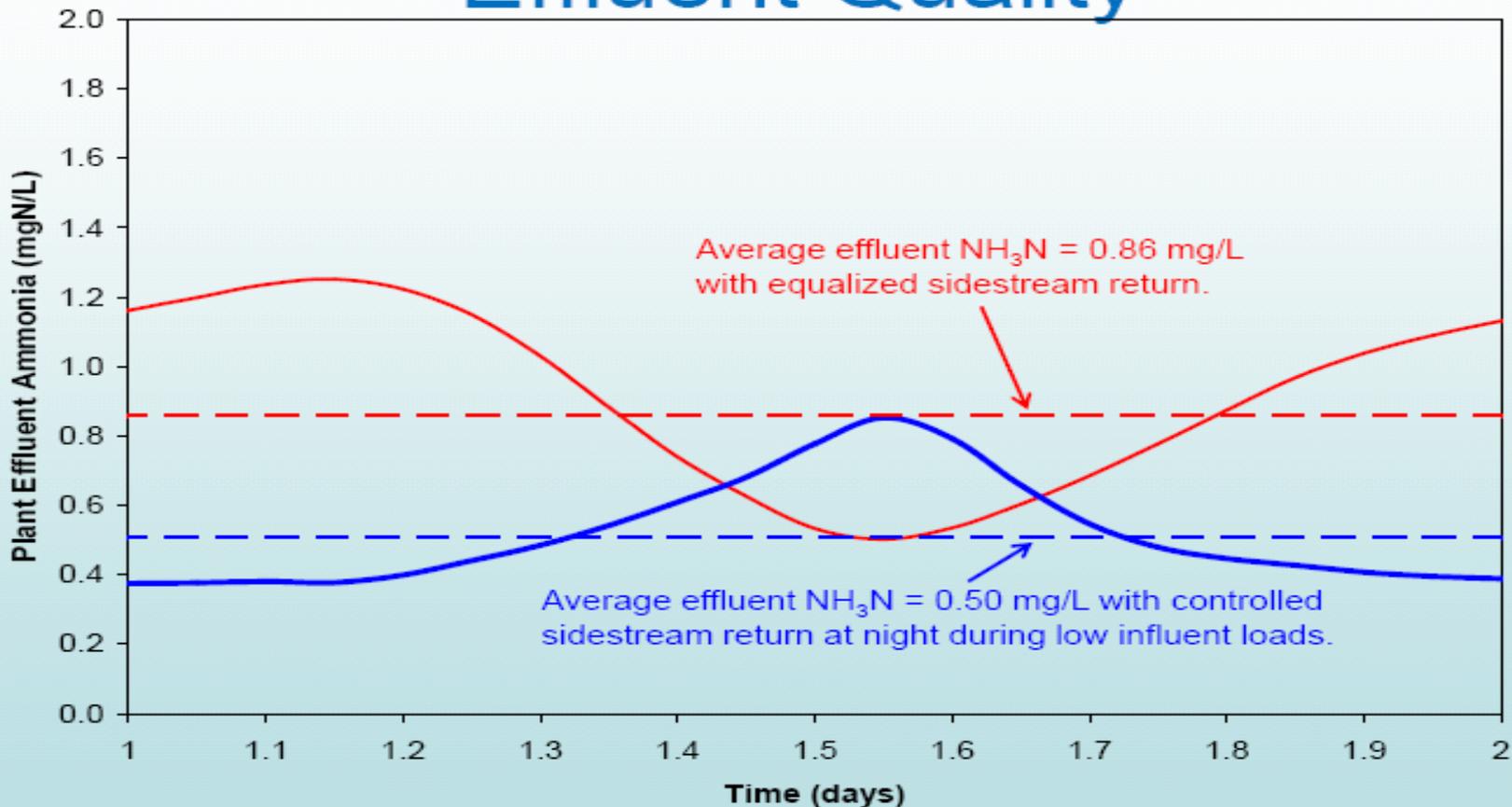


THE OPTIONS

- 1. Maintain Present Operation**
- 2. Recirculate But Equalize the Flows**
- 3. Use As a Liquid Fertilizer**
- 4. Remove or Recover Nutrients**

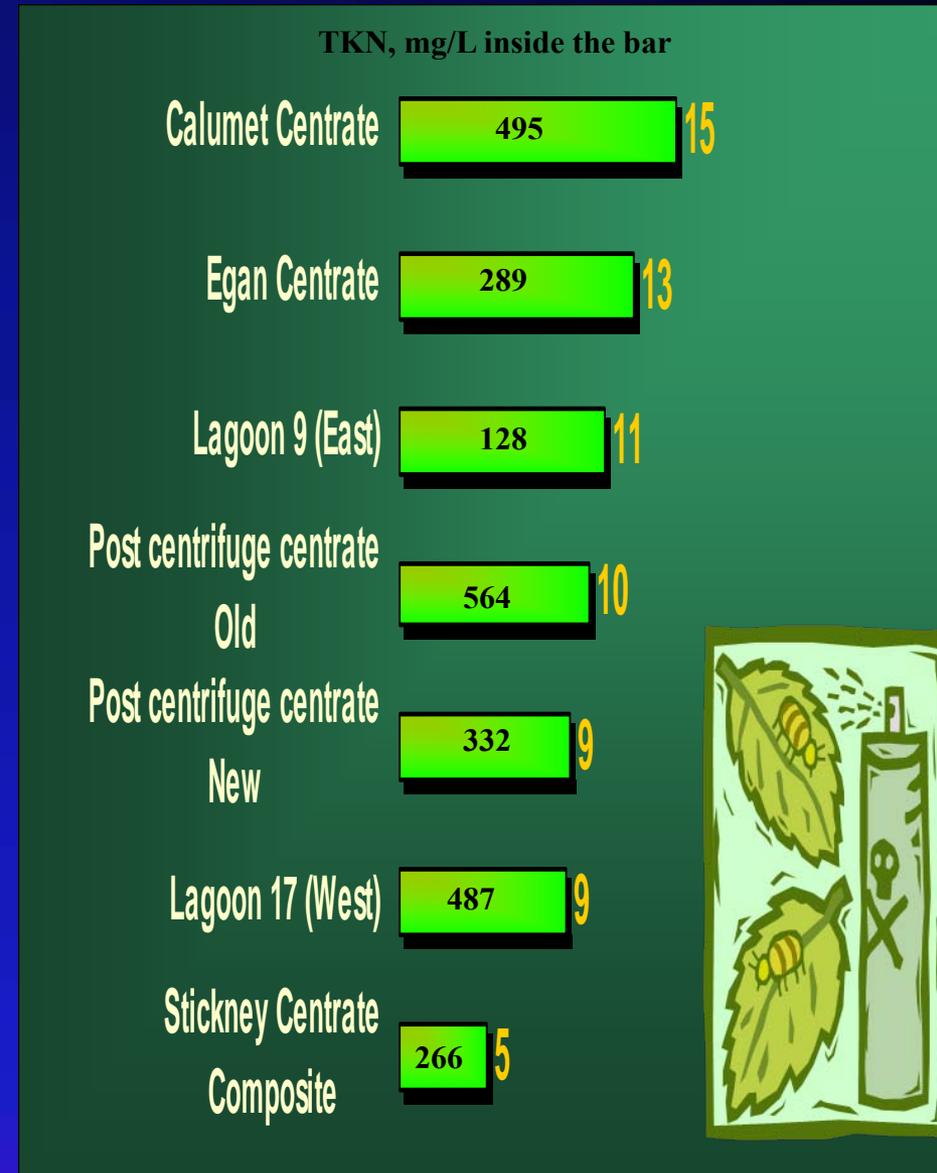
OPTION 2: CONCEPTUAL REPRESENTATION OF RECYCLE FLOW EQUALIZATION

Sidestream Control Impacts Effluent Quality



OPTION 3: LIQUID FERTILIZER (N:P :: >5 to 1)

- A total of 18 MGD (37% flow) from 7 streams out of 13
- Benefits to the Environment
 - Conserve water/phosphate reserves
 - Recycle materials locally
 - Avoid greenhouse gas emissions (~8 tons CO₂e per ton fertilizer produced)
 - Environmental Sustainability
- Drawbacks
 - Transport based on volume required
 - Heavy metals



OPTION 3: AN OFFICIAL SEAL OF APPROVAL FOR LIQUID FERTILIZER



OPTION 4A: TREAT TO REMOVE
NUTRIENTS. WHY?

OPTION 4B: TREAT TO RECOVER
NUTRIENTS. WHY?

Option 4A: Why to Treat Recycle Streams?

1. Stringent Regulatory Limitations
 - **TP (Water Quality)**
 - **TN (Water Quality)**
 - **Nitrate (SDWA)**
 - **NH₃-N (NPDES for Aquatic Toxicity)**
 - **Bottle-necks in Permit (Daily Max, Wkly Avg. etc.)**
2. Sustainable Treatment for Nutrient Removal & Entire Plant
 - **Requires less energy (reduction in C footprint)**
 - **Increases Process Capacity at Low Temperatures**
3. Common Treatment for Multiple Plants
 - **More TP and TN @ SWRP from NSWRP/EWRP**
 - **Less Capital & OM Costs**
 - **Reliable Operations @ One Location than Two Small-scale Operations**
4. Adjustment in Plant Operations
 - **Variable Thickening and Dewatering Process Schedule**
 - **Impact if Only One Shift or Certain Days (HPWRP, CWRP)**
 - **Increased use of BNR**
 - **Major Plant Upgrade (e.g. Master Plan)**

Option 4B: Why to Recover Nutrients?

FACTS AND PERSPECTIVE ON P

–Phosphorus Supply Challenges

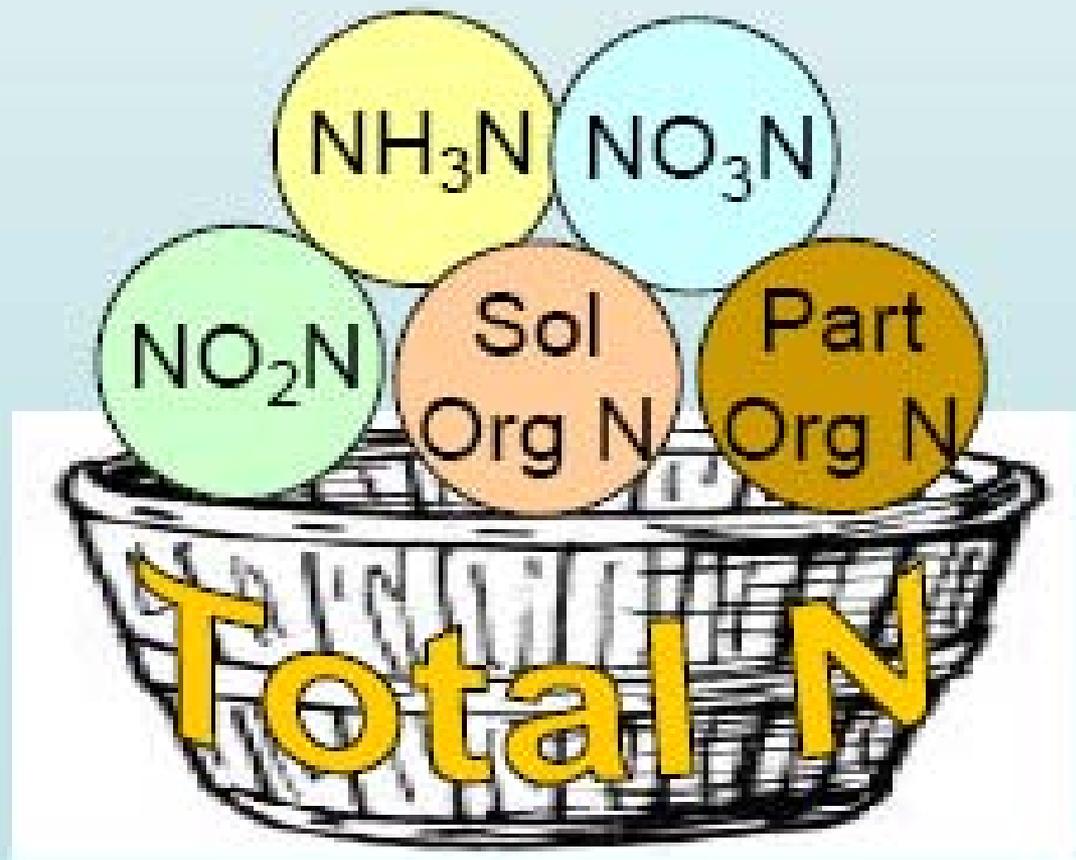
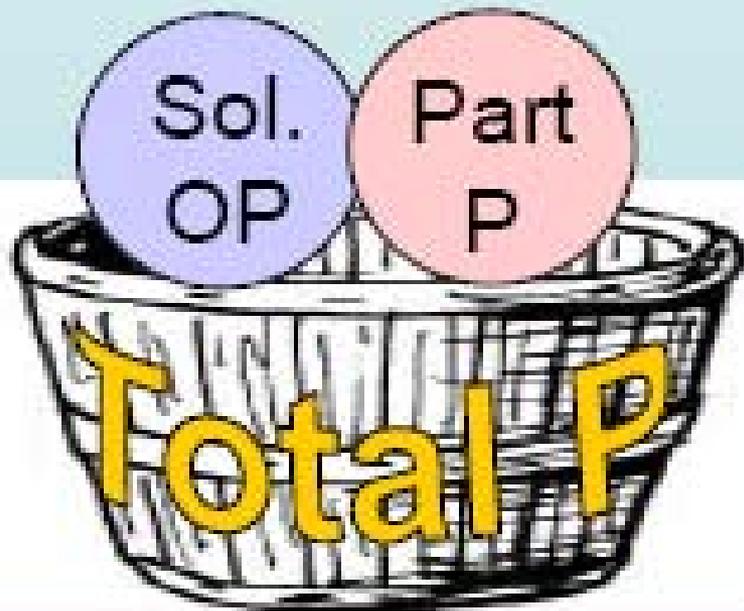
–Nutrient Recovery from a global perspective (7 billion humans and 63 billion live stock)

–1.5% mining of rock phosphate can be reduced if P recovery around the world (Shu et. al. 2006)

–“We may be able to substitute nuclear power for coal, and plastics for wood, and yeast for meat, friendliness for isolation – but for phosphorus there is neither substitute nor replacement” Isaac Asimov

–Conserve phosphate reserves, recycle P locally, reduce GHGs and environmentally sustainable

Treatment Technologies for Options 4A and 4B



TREATMENT TECHNOLOGIES

Biological

- CND
- AND : Bioaugmentation w/ and w/o RAS (In-Nitri, BABE, BAR etc.)
- Nitritation/Denitritation and Deammonification (SHARON, ANNAMOX, SBR, STRASS, MAUREEN, OLAND, CANON etc.)
- Algae Based (stabilization/oxidation ponds, Algaewheel®, Algal Turf Scrubber® Technology, Algae farms)

Physicochemical

- Ammonia Stripping (ARP via Steam, Hot Air, & CAST Vacuum Distillation)
- IE
- MAP based technologies (Metal Salts, Ostara, Pro-Corp)

SCREENING OF TECHNOLOGIES

- CND: Alkalinity deficiency 25, 88, 82% at CWRP, EWRP and SWRP, respectively, impact on aeration cost, ammonia toxicity etc.
- Bioaugmentation: pH, temp, TDS/osmotic pressure changes in main treatment so augmented nitrifiers predated
- Nitritation/Denitritation/Deammonification: Many premature and emerging technologies - not suitable for full-scale of District plants
- Algae Based: Settling and possible SS violation, premature for full-scale, polymer costs
- Air Stripping: 2000:1 Air to NH₃ ratio, pH ~11, ~55C air temp – pH and temp control, scaling etc.
- Steam Stripping: Heat exchanger & stripper fouling, 300 - 500 to 1 steam to liquid ratio, high temp maintenance and associated energy cost
- IE: Pretreatment such as filtration needed, salt deposits within resin bed, piping etc.

NITRIFICATION, NITRITATION-DENITRITATION AND DEAMMONIFICATION FUNDAMENTALS

- CND: Alkalinity – 7.14 g/g NH₄
 - : O₂ – 4.57 g/g NH₄
 - : C – 3 to 4.5 g COD/g of NO₃

Nitritation/Denitritation:

- : O₂ – 25% less wrt CND
- : C – 40% less so 40% less biomass

•Deammonification:

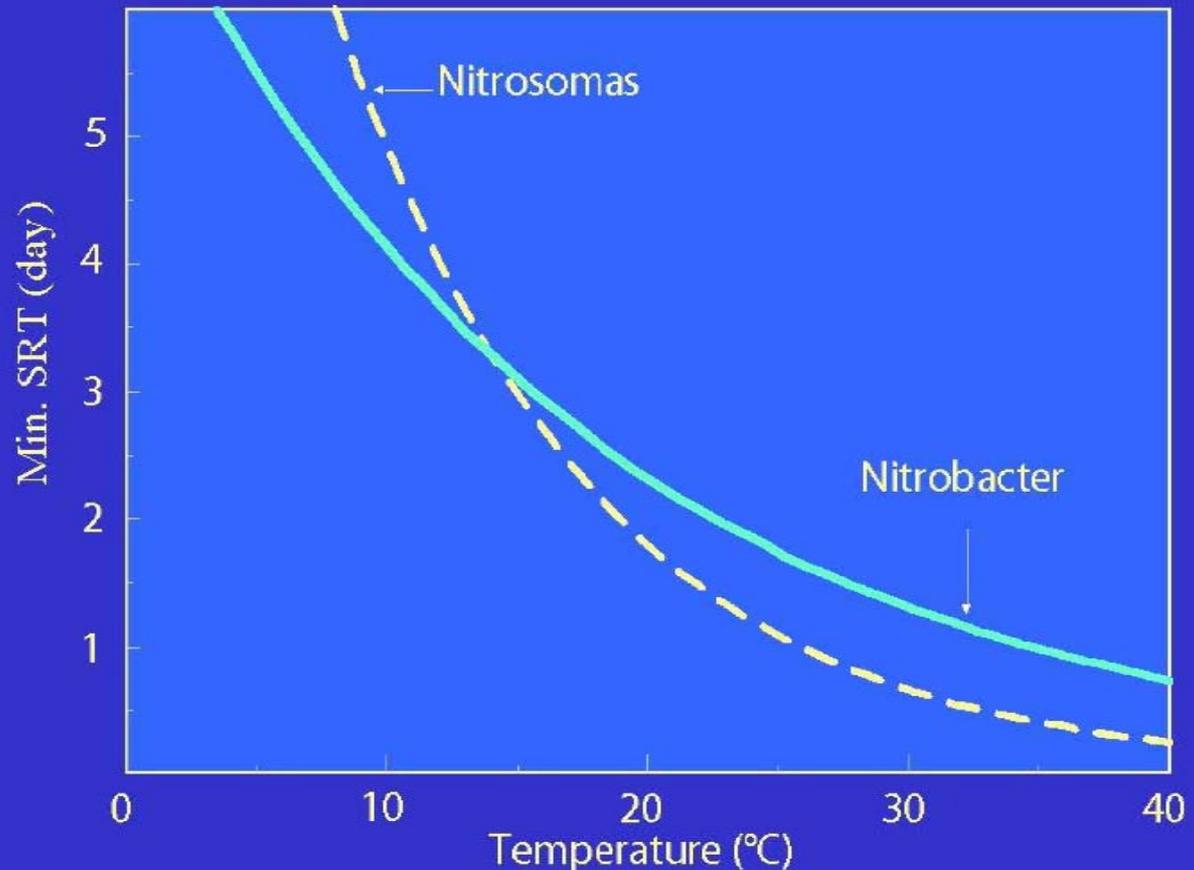
- : O₂ – 62% less wrt CND
- : C – 100% less so much reduced biomass
- : Reduced CO₂ and N₂O

SINGLE REACTOR FOR HIGH ACTIVITY AMMONIA REMOVAL OVER NITRITE

Features:

- At 25-40 C the nitrifying bacteria have a higher growth rate than the nitrifying bacteria.
- pH 6.6 to 7.2 for AOBs and DO 0.3 to 2 mg/L
- SRT=HRT
- At a 1 day SRT/HRT the reactor acts as a selector converting ammonia to nitrite
- The process then allows for denitrification via nitrite.

BIOLOGICAL GROWTH RATE – SRT_{MIN} AS A FUNCTION OF TEMPERATURE



SHARON PLANTS

| Location | Nitrogen Capacity(pe) | (lbs N/day) | Operation |
|------------------------------|----------------------------------|--------------------|------------------|
| Utrecht, Netherlands | 400,000 | 2000 | 1997 |
| Rotterdam-Dokhaven | 470,000 | 1900 | 1999 |
| Zwolle | 200,000 | 900 | 2003 |
| Beverwijk | 320,000 | 2,600 | 2003 |
| Groningen-Garmerwolde | 300,000 | 5,300 | 2004 |
| Den Haag-Houtrust | 430,000 | 2,900 | 2004 |
| New York-Wards Island | 250 MGD | 12,700 | 2008 |
| Geneva, Switzerland | 115 MGD | 3,600 | 2009 |



Images courtesy of Grontmij NV



Image courtesy of Grontmij NV

WARDS ISLAND, NEW YORK SHARON PLANT

- Goals:**
- To reduce TN discharge from the Wards Island facility into the East River/Long Island Sound/NY Harbor
 - To reduce TN discharge associated with the solids handling at multiple NYC-DEP facilities
 - To utilize a highly efficient process for cost savings associated with TN



Images courtesy of Grontmij NV



WARDS ISLAND, NEW YORK – 250 MGD

Solids from 3 Plants

First in the USA and the largest in the world

Two Parallel SHARON Reactor Trains :

Design / Peak Flow : 1.85 / 2.31 MGD

**NH₃ : 700 mg/l
10,800 lbs./day
(~30% N-Load)**

TSS : 600 mg/L

COD : 950 mg/L

Temp. : 28 – 32 C

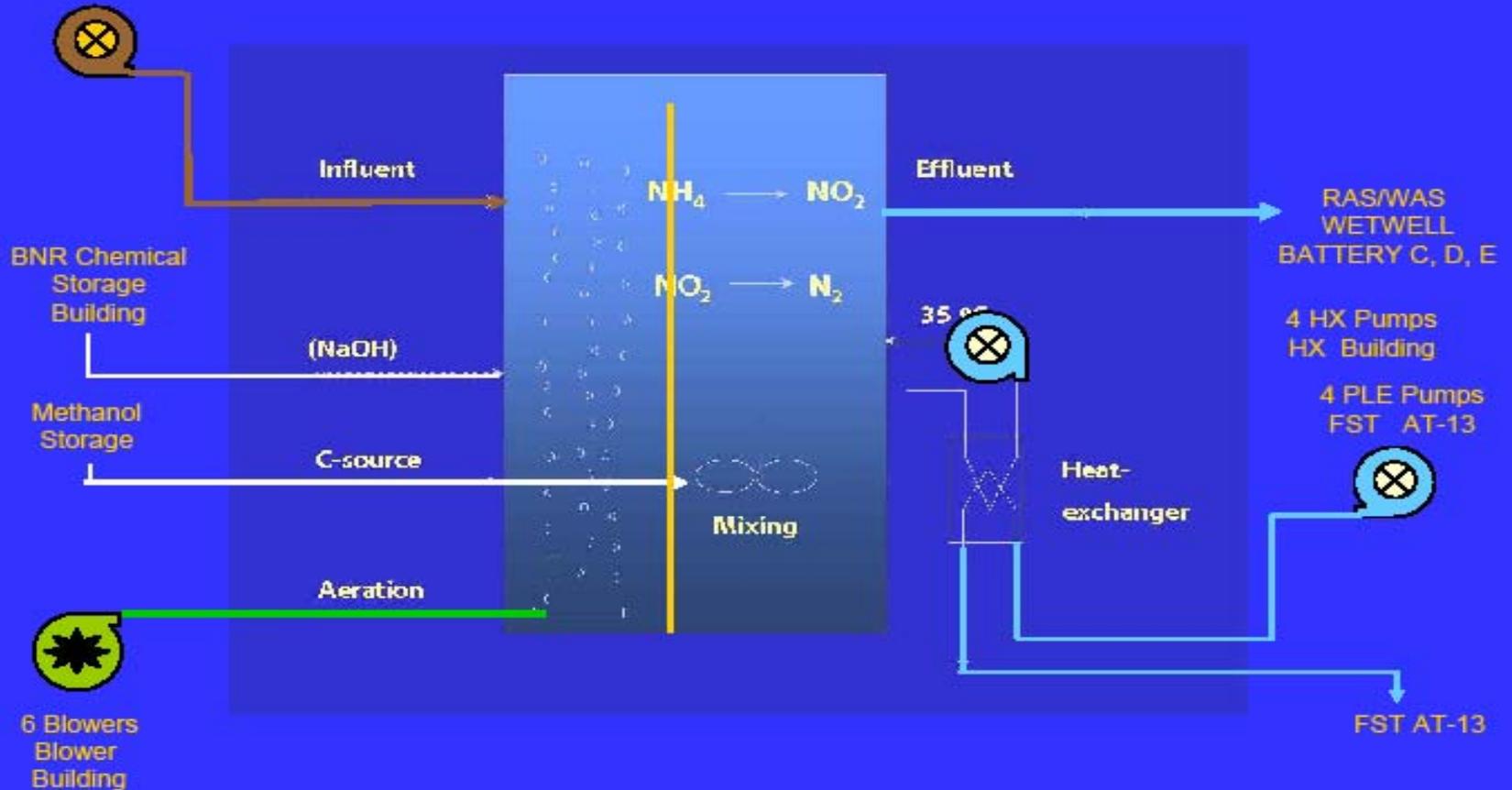
N-Removal : >95%

Benefits:

- Removes 25-35% of ammonia load to main stream nitrification tanks. Over 2.5 tpd TN removed.
- Reduces oxygen required for nitrification by 25%. Lowering both capital and M&O costs.
- Reduces methanol required for denitrification by 40%. Lowering both capital and M&O costs.
- Reduces the size of main stream reactors, especially associated with respect to denitrification processing.

3 Centrate Pumps
Dewatering
Building

Wards Island SHARON® System



Courtesy of Mr. Keith Beckmann, P.E., Chief - Process Planning of NYCEP, NEW YORK

ANaerobic AMMonium OXidation Process

- Observation of simultaneous removal of $\text{NH}_4\text{-N}$ and production of N_2 in the Netherlands in 1986 led to ANAMMOX technology
- A derivative of SHARON process - ANAMMOX bacteria/autotrophic bacteria accomplish N-removal during nitrification & denitrification
- $\text{NH}_4\text{-N}$ is used as an electron donor in lieu of organic carbon source such as methanol
- 50 % of $\text{NH}_3\text{-N}$ is oxidized to $\text{NO}_2\text{-N}$ in a SHARON reactor and equal ratio of $\text{NH}_4\text{-N}$ to $\text{NO}_2\text{-N}$ liquor is sent to the second ANAMMOX reactor, where the ANAMMOX bacteria reduce nitrite to N_2
- Both processes can take place in a single reactor where two guilds of bacteria form compact granules (Kartal et. al. 2010)

Enriched culture of anaerobic ammonium oxidizing bacteria
(Radboud University Nijmegen) [Kinestetika](#) 20:44, 15 August 2007 (UTC)



anammox reactor, KU Nijmegen

ANAMMOX Process Benefits (STOWA)

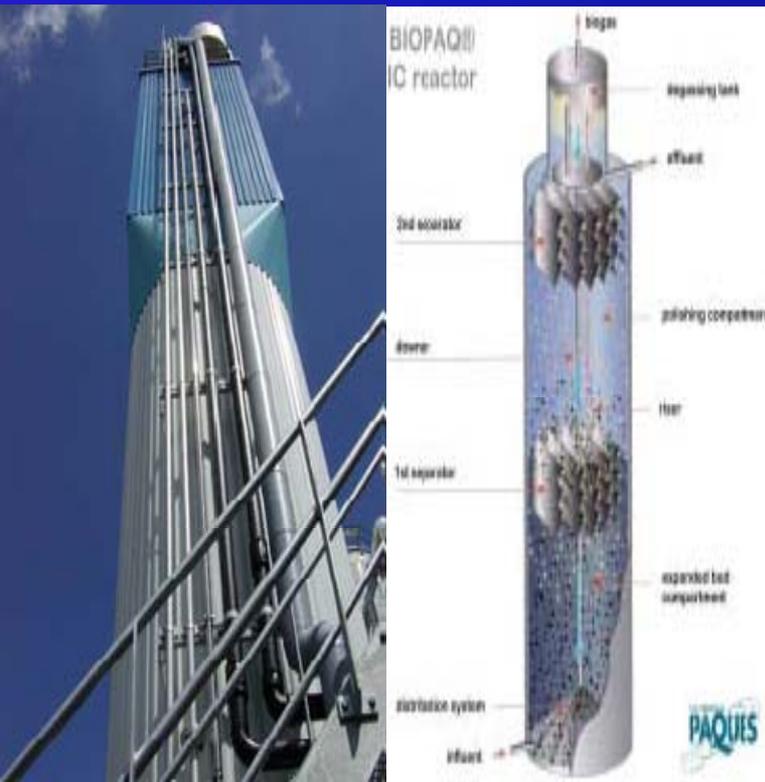
- **62% Reduction in O₂ wrt conventional nitrification to nitrate**
- **No organic carbon needed for denitrification**
- **Reduced biomass production**
- **Operating costs reduction by 90% compared to CND (van Loosdrecht, 2004)**
- **Reduction in GHG gases by 95% possible because of the consumption of CO₂ and a lack of production of nitrous oxide (N₂O)**
- **N₂ gas can partially mix the contents which can reduce the mixing energy needs**
- **Sustainable process wrt economic and operational perspectives**

ANAMMOX Process Full-scale Applications and Challenges

- The DCWASA, City of Baltimore and the NYCDEP spent considerable effort on this technology, DCWASA under design stage for sidestream

- As of 2010, 20 installations in Europe and 2 in design in the US

- A full-scale test for raw sewage to begin in Strass Austria and pilot-scale at HRSD



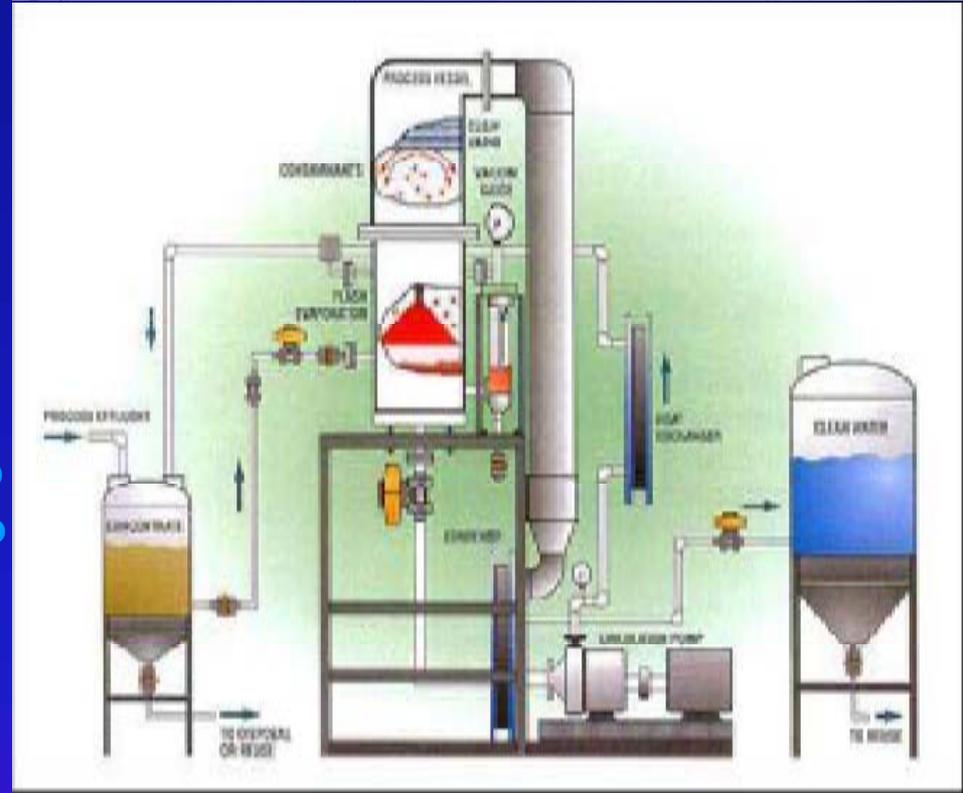
- Very slow growth rate of ANAMMOX bacteria need 100 to 200 days after initial seeding to reach full capacity and produce low sludge production. Due to slow growth rate, sludge retention is very important and typical SRT is 1.5 to 2 days

- Higher nitrite concentration for extended period of time is detrimental to ANAMMOX bacteria

- Challenge is to make it suitable for the treatment of wastewater with lower nitrogen concentrations and low temperatures.

Controlled Atmosphere Separation Technology Vacuum Distillation (CASTion)

- CASTion – A subsidiary of ThermoEnergy
 - Proprietary tech for recovery of chemicals and water in many industries including WRPs
 - Up to 40% NH_3 recovery as NH_4SO_4
 - Flash Vacuum Distillation
 - Atomizer
 - Low Vacuum
 - Continuous or batch
 - **Physical principles**
 - Uses partial pressures to separate materials
 - Uses sensible heat of wastewater to increase efficiency
 - Combined with other technologies (IE, MBR etc) depending on application
- Key Variables :** pH (10 to 12), feed temp (90 to 120 F, pressure –ve 26 to 29”, process time 6 to 12 min, recirculation rate 15 to 30 turnovers



CASTion PILOT-SCALE RESULTS

- **Midsized Aberdeen, WA filtrate: 80% of initial NH_3 of 550 ppm in 7 min at 11.5 pH and T 100 to 120 F**
- **NYCDEP 26th Ward centrate pilot tests: 80% of initial NH_3 of 815 ppm in 3 min at >12 pH and T 90 F**
- **Also maintained <100 ppm effluent NH_3 from the initial 550 ppm for 28 min at 11.2 to 11.4 pH and T 100 F**
- **1.2 MGD centrate CASTion project at 26th Ward plant to begin Qtr 2, 2010.**
- **City of Tacoma, WA is to start on-site pilot tests for \$50,000 (Off-site tests for \$3 to 4000)**

Benefits and Drawbacks / Limitations :

- **+ Potential for substantial reduction in methanol requirement for BNR because it returns alkalinity and COD for BNR**
- **- Filters, IE pretreatment, pH and temp increase make it costly depending upon centrate quality**

STRUVITE – A BUILDING BLOCK FOR MAP BASED TECHNOLOGIES



**SEWER PIPES
FROM
EPHESUS
(FOUNDED
300 B.C.)**

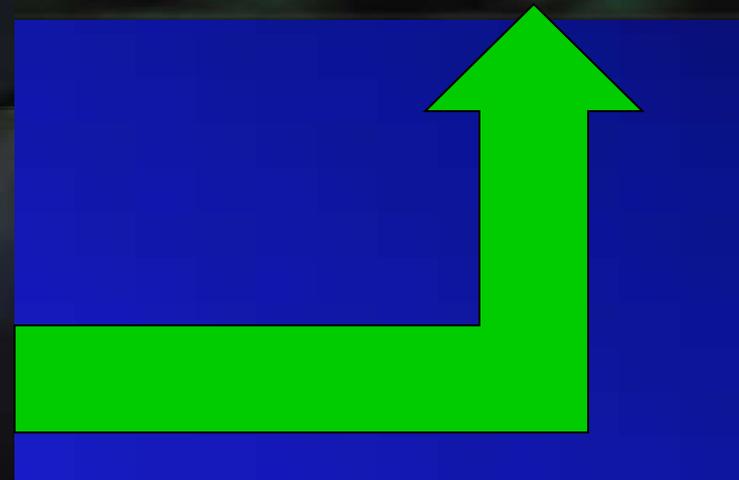
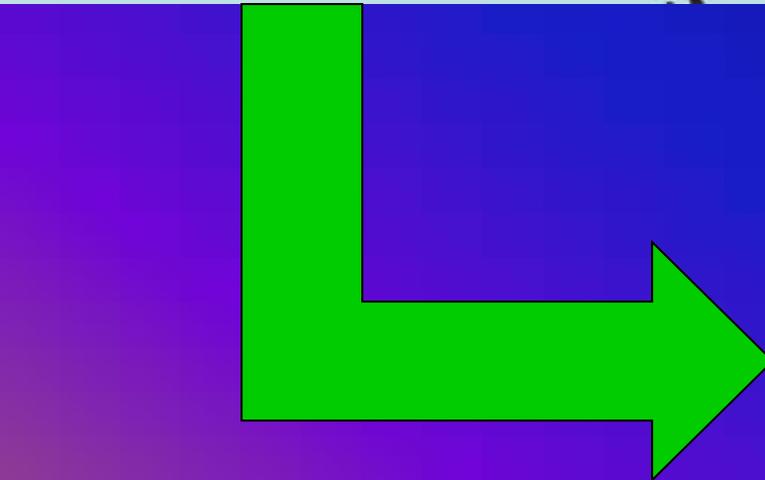
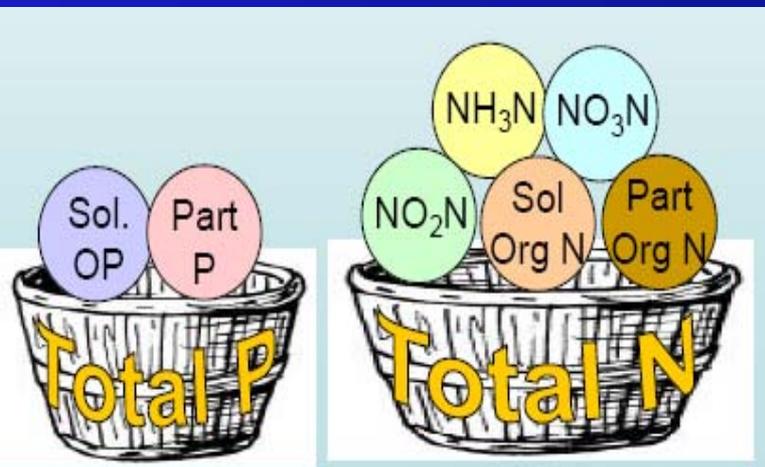


- pH dependent, pH pushes the reaction. $\text{CO}_2 \uparrow = \text{pH} \uparrow = \text{struvite} \downarrow$
- Removes equi-molar ammonia and phosphorus
- AKA: Struvite, MAGamp, MAP
- Mg limiting element

1 kg of struvite can be recovered from 100 m³ wastewater & applied on 2.6 ha arable land (Shu L. et. al.)

MAP Based Technologies for P Recovery from Resource Streams

OSTARA & PROCORP, LLC



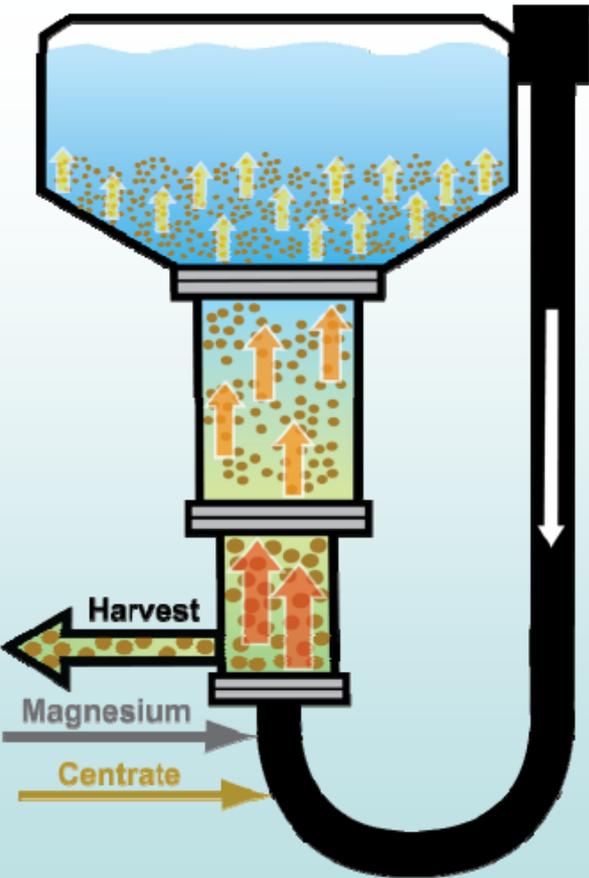
Pilot-scale Prills



Full-scale Prills



PEARL™ Process Operation



OSTARA NUTRIENT RECOVERY TECHNOLOGIES INC.

PREFERRED APPLICATION

- Plant size >5 MGD
- Plant processes:
 - Anaerobic zone (Bio-P)
 - Anoxic zone for denitrification/biological selectors
 - Anaerobic digestion & dewatering
- PEARL™ process feed stream desired characteristics:
 - $\text{PO}_4\text{-P}$ >75 mg/L, and > 140 lbs/day for 90% + P removal
 - TSS <1000 mg/L
- Struvite and/or vivianite formation challenges
- <10 Year Payback / Instant Net Savings
- At present, not feasible at District plants but may become feasible with Bio-P treatment

OSTARA TREATMENT AT DISTRICT WRPS

- NOT FEASIBLE DUE TO LOW P**
- BIO-P IS A MUST**
- IN ORDER TO REALIZE CASH FLOW, NEEDS AT LEAST 2 TO 3 TIMES HIGHER P IN CENTRATE**

Estimated P-Recovery at Stickney, Egan and Calumet WRRPs : Pro-Corp LLC

| Recycle | Fertilizer, tpd | NH₃, lbs/day | TP, lbs/day |
|--------------------------------------|------------------------|--------------------------------|--------------------|
| SWRP Pre-Centrates | 6 | 740 | 1600 |
| SWRP Pre & Post Centrates | 11 | 1500 | 2700 |
| EWRP Centrate + Filtrate | 0.33 | 46 | 83 |
| CWRP Centrate | 0.2 | 26 | 48 |
| CWRP Lagoon 9 (Not enough P) | --- | --- | ---- |
| Lagoon 17 | 0.4 | 48 | 87 |

If Iron is not added at EWRP, more P will be available, potentially up to 75% of TP

A SUMMARY OF TREATMENT TECHNOLOGIES FOR FURTHER CONSIDERATION AT DISTRICT WRPS

- **SHARON-ANNAMOX process for SWRP**
- **Consider CASTion based on cost economics if excess recovered by-product can be sold in Chicago markets**
- **Consider MAP Based Technology if Bio-P is implemented : Ostara or ProCorp LLC**
- **Keep eye on Algalwheel success**

THE NEXT STEP

- **Need for data on flow and characteristics of recycle streams**
- **Due to limited supply of P, P-resource recovery from recycle streams in future may become more attractive**
- **Identify and evaluate feasibility of select technology (e.g. SHARON-ANAMMOX at SWRP) at a pilot-scale**

THANKS FOR YOUR ATTENTION

- Questions and/or Comments Now?
- Later? kamlesh.patel@mwrdd.org
 - 708-588-3735

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