



The Metropolitan

Water Reclamation District

of Greater Chicago

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TO THE AUGUST EDITION
OF THE 2012
M&R SEMINAR SERIES**

BEFORE WE BEGIN

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- Home Page ⇒ (Public Interest) ⇒ more public interest ⇒ M&R Seminar Series ⇒ 2012 Seminar Series
- SEMINAR VIDEO IS STREAMED ON-DEMAND AND CAN BE ACCESSED FROM www.MWRD.org website via RSS Feed

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Engineers Without Borders – UCLA, UCI, LA, and OC chapters (2004 – present)

Engineering Intern, the City of Los Angeles, Bureau of Sanitation (2001)

Education : M.S. equivalent, University of Padua, Italy, Chemical Engineering
Laurea

M.S. / Ph.D. University of California, Los Angeles , Environmental Engineering,

Professional: American Academy of Environmental Engineers,

Water Environment Federation,

International Water Association,

Association of Environmental Engineering and Science Professors,

Engineers Without Borders.

Honors &: American Academy of Environmental Engineers: Research Honor Award (2011)

OXYGEN TRANSFER IN WASTEWATER TREATMENT PROCESSES: RESEARCH PERSPECTIVES IN THE 21ST CENTURY



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Department of Chemical Engineering and Material Science

MWRDGC Monthly Seminar
Stickney Water Reclamation Plant

August 24th, 2012



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I. EFFECTS OF WASTEWATER CONTAMINANTS ON OXYGEN TRANSFER

Terminology

OTE: Oxygen Transfer Efficiency (%)

OTR: Oxygen Transfer Rate ($\text{kg}_{\text{O}_2}/\text{h}$)

SOTE: Standardized OTE in clean water (%)

α SOTE: Standardized OTE in process water (%)

$\alpha = \alpha\text{SOTE}/\text{SOTE}$ (water quality estimate)

$F = \text{Fouling factor} = \alpha\text{SOTE}_{\text{old}} / \alpha\text{SOTE}_{\text{new}}$

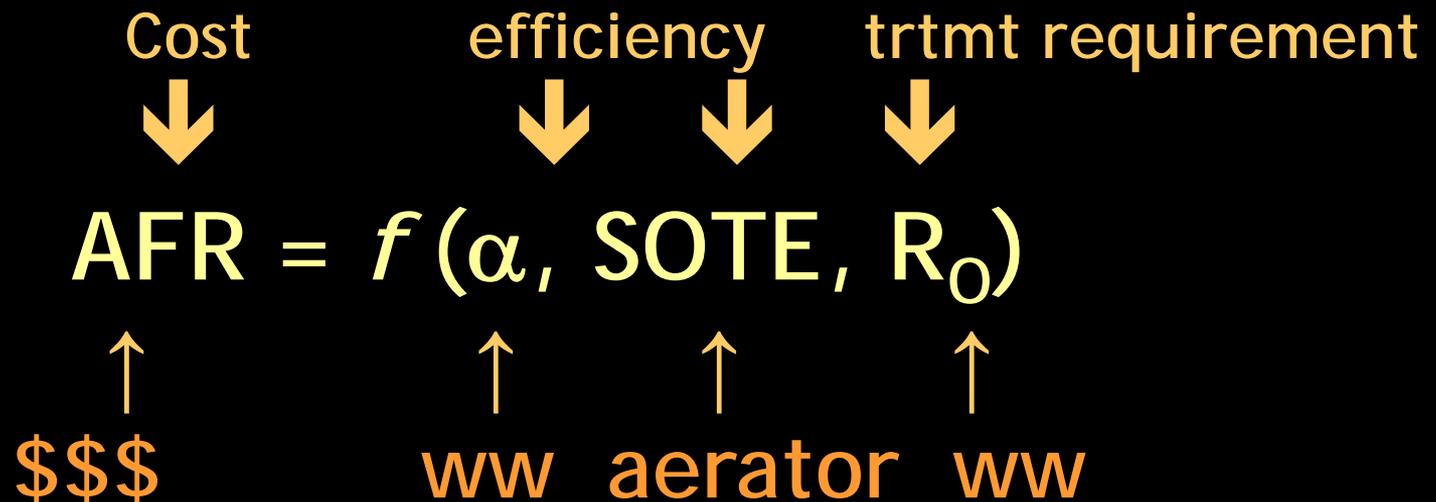
DWP = Dynamic wet pressure (diff. headloss, Pa)

$\Psi = \text{Pressure factor} = \text{DWP}_{\text{old}} / \text{DWP}_{\text{new}}$

α : THE MOTHER OF ALL “FUDGE” FACTORS

$$\alpha = \frac{(k_L a)_{\text{process water}}}{(k_L a)_{\text{clean water}}}$$

SOTE = Standardized Oxygen Transfer Efficiency
(O₂ transferred / O₂ fed)



WHAT ARE THESE CONTAMINANTS?



CONTAINS:

**15-25% anionic
surfactants**

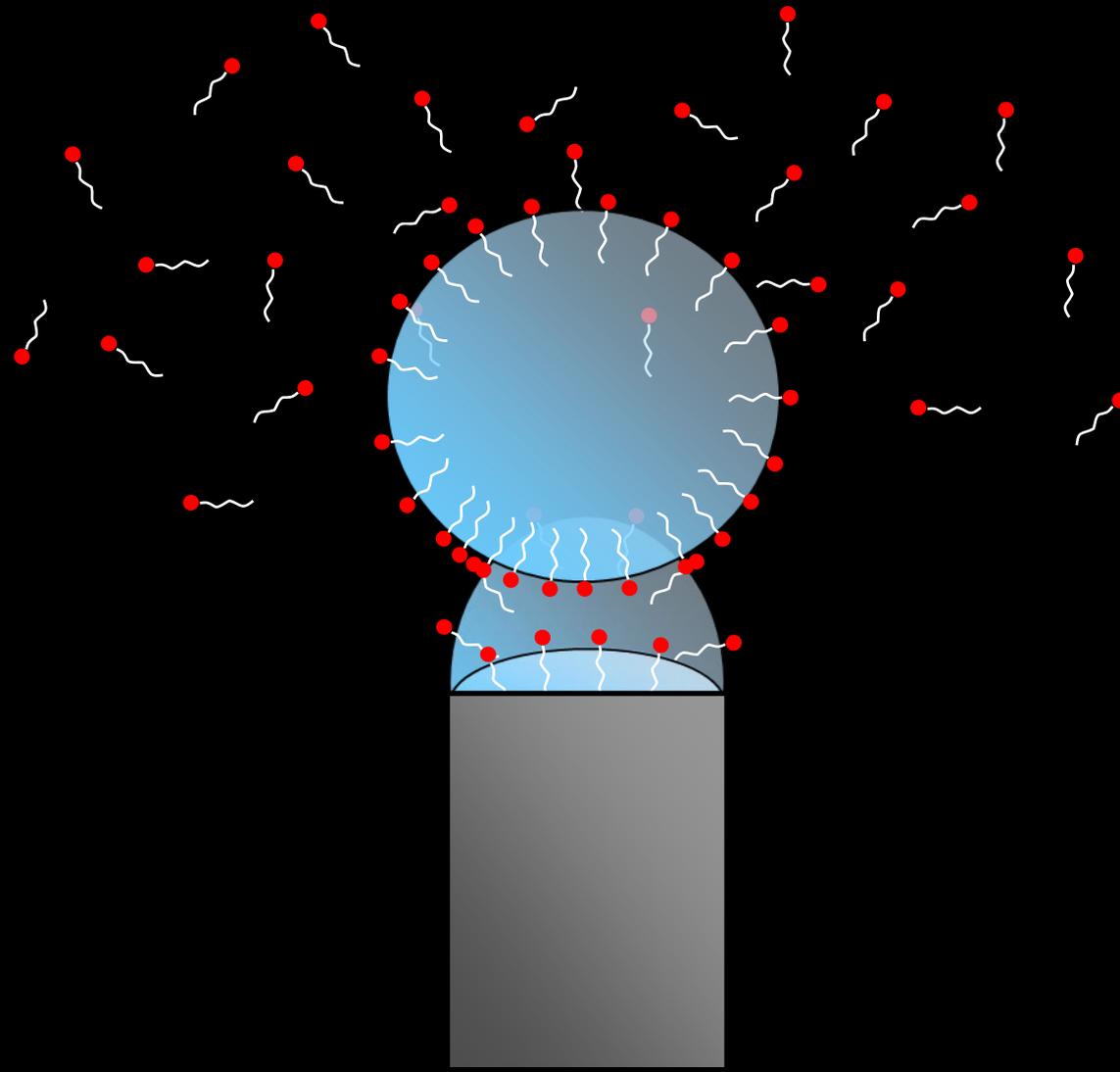
**0-15% non-ionic
surfactants**

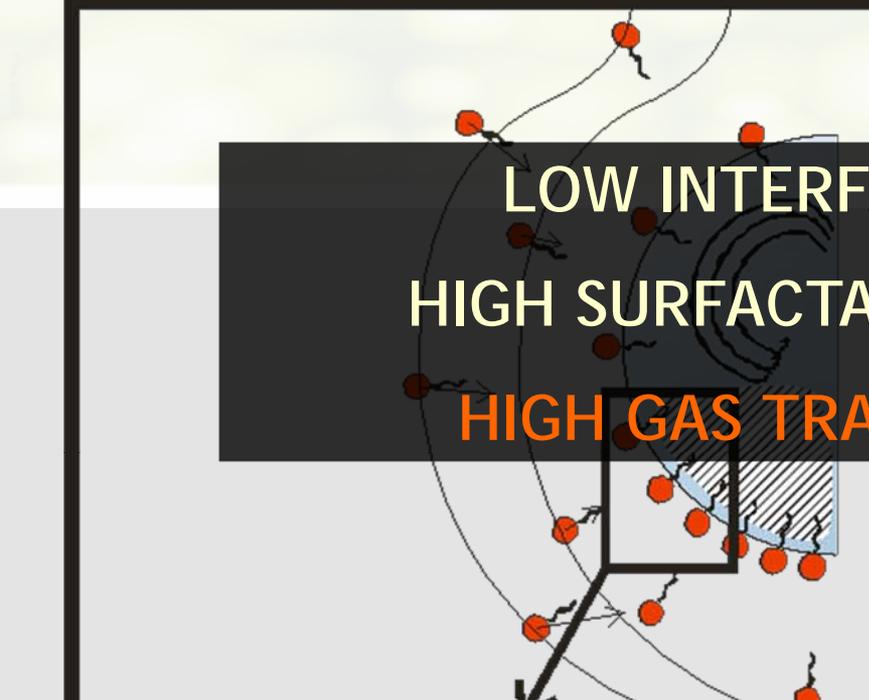
0-15% soap

**0-15% cationic
surfactants**

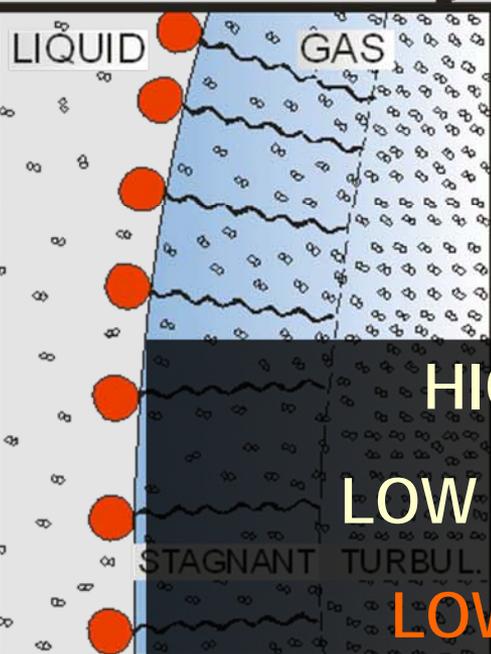
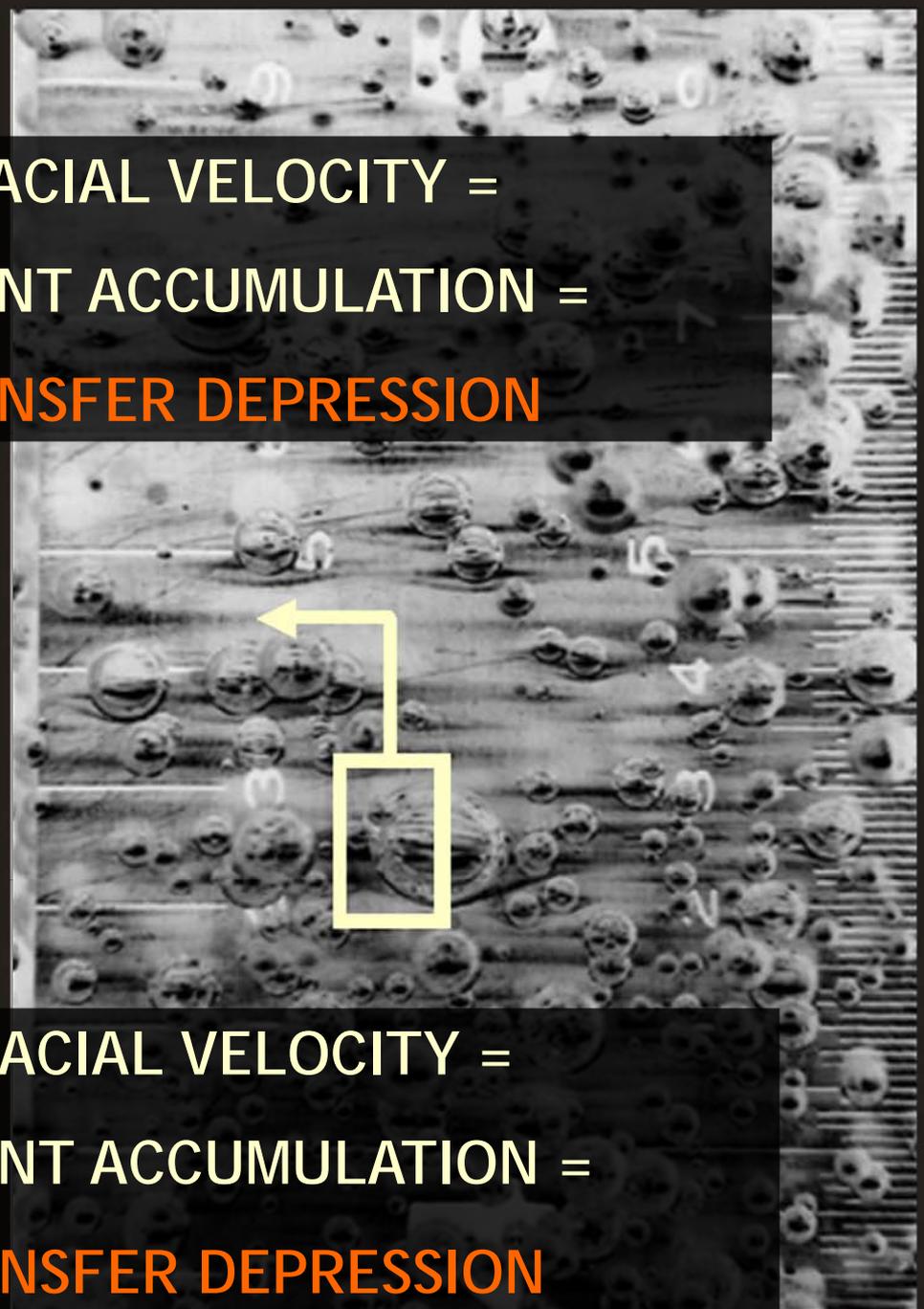
fillers to 100%

SURFACTANT INTERFACIAL ACCUMULATION



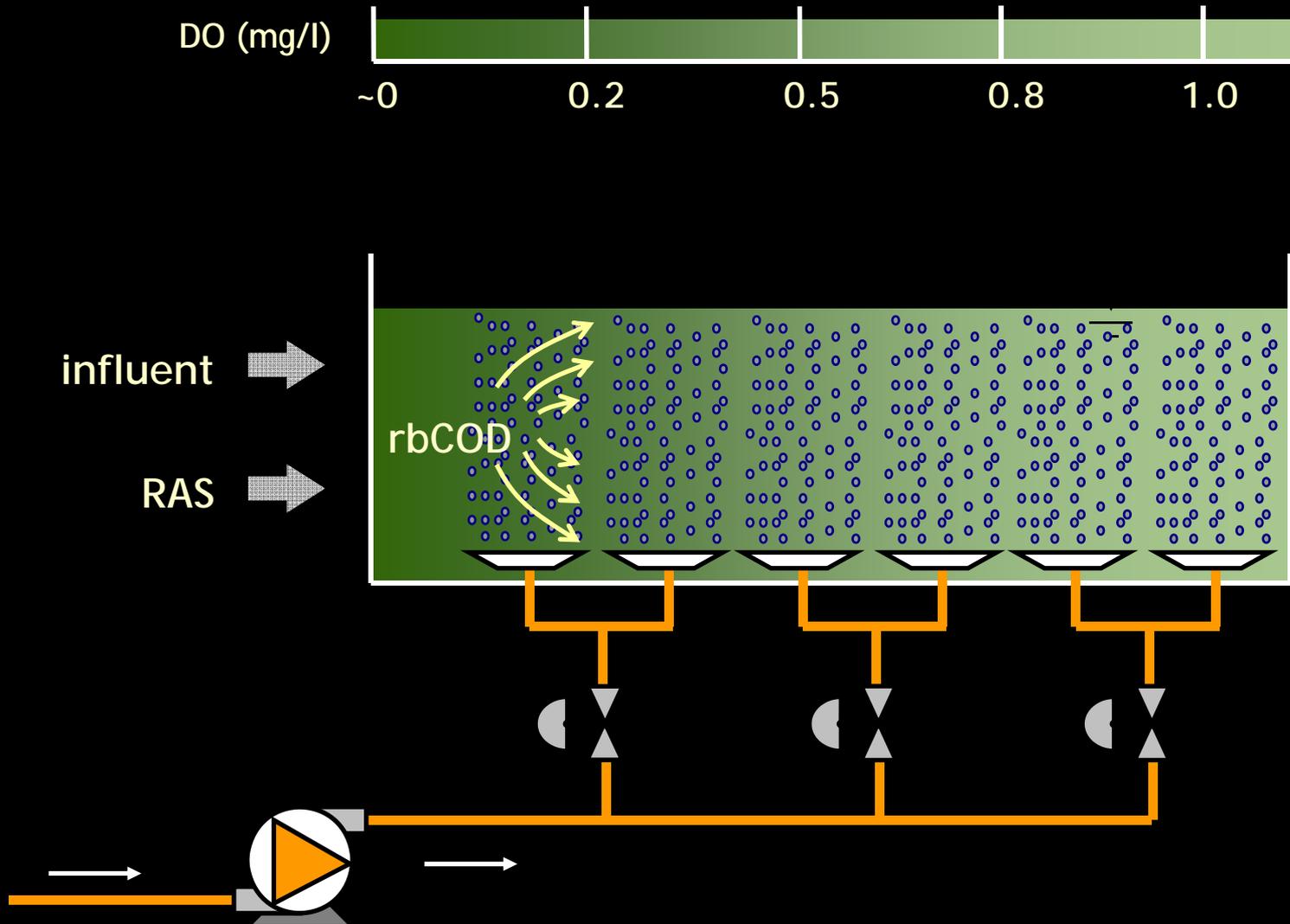


**LOW INTERFACIAL VELOCITY =
HIGH SURFACTANT ACCUMULATION =
HIGH GAS TRANSFER DEPRESSION**

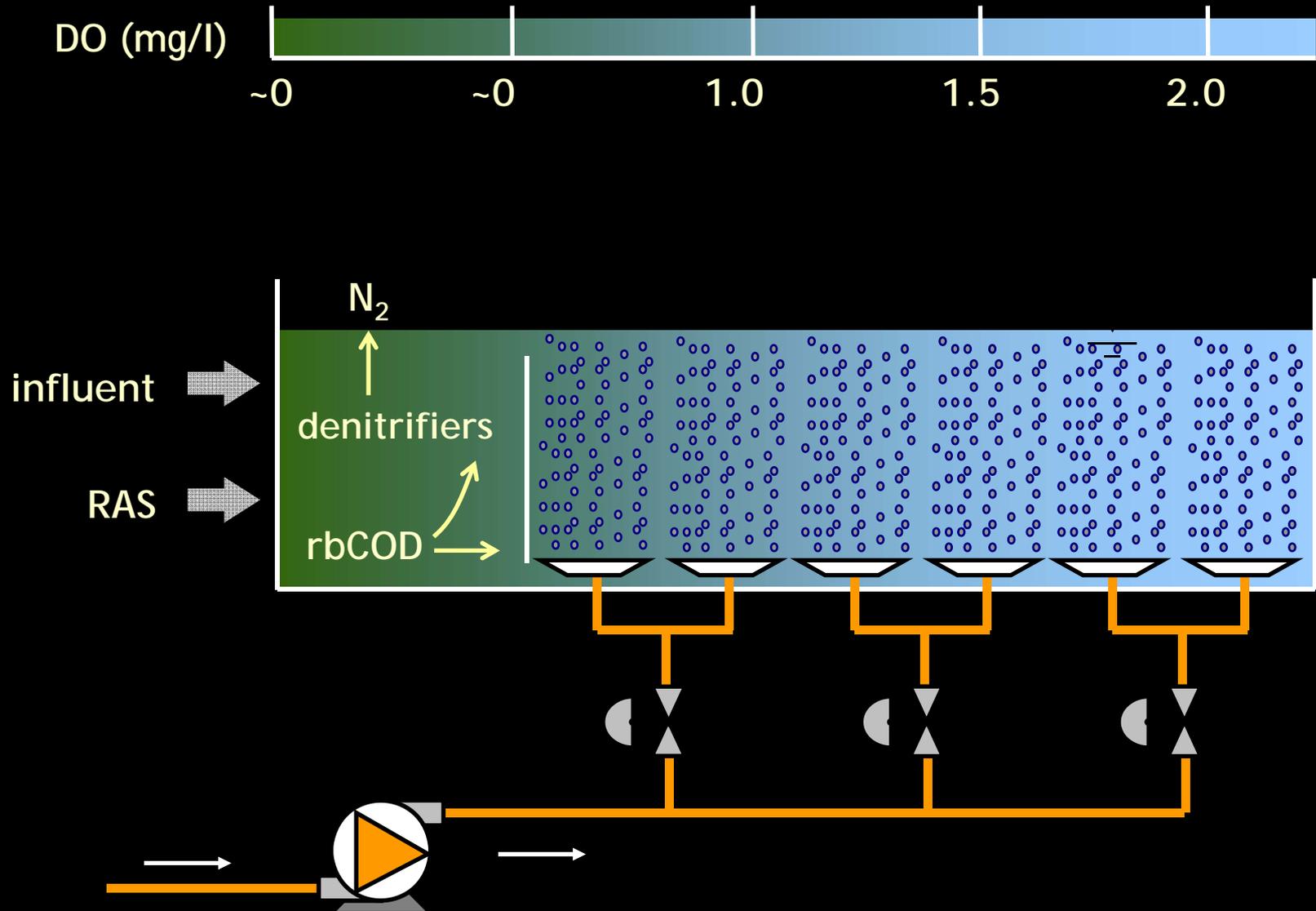


**HIGH INTERFACIAL VELOCITY =
LOW SURFACTANT ACCUMULATION =
LOW GAS TRANSFER DEPRESSION**

CONVENTIONAL LAYOUT

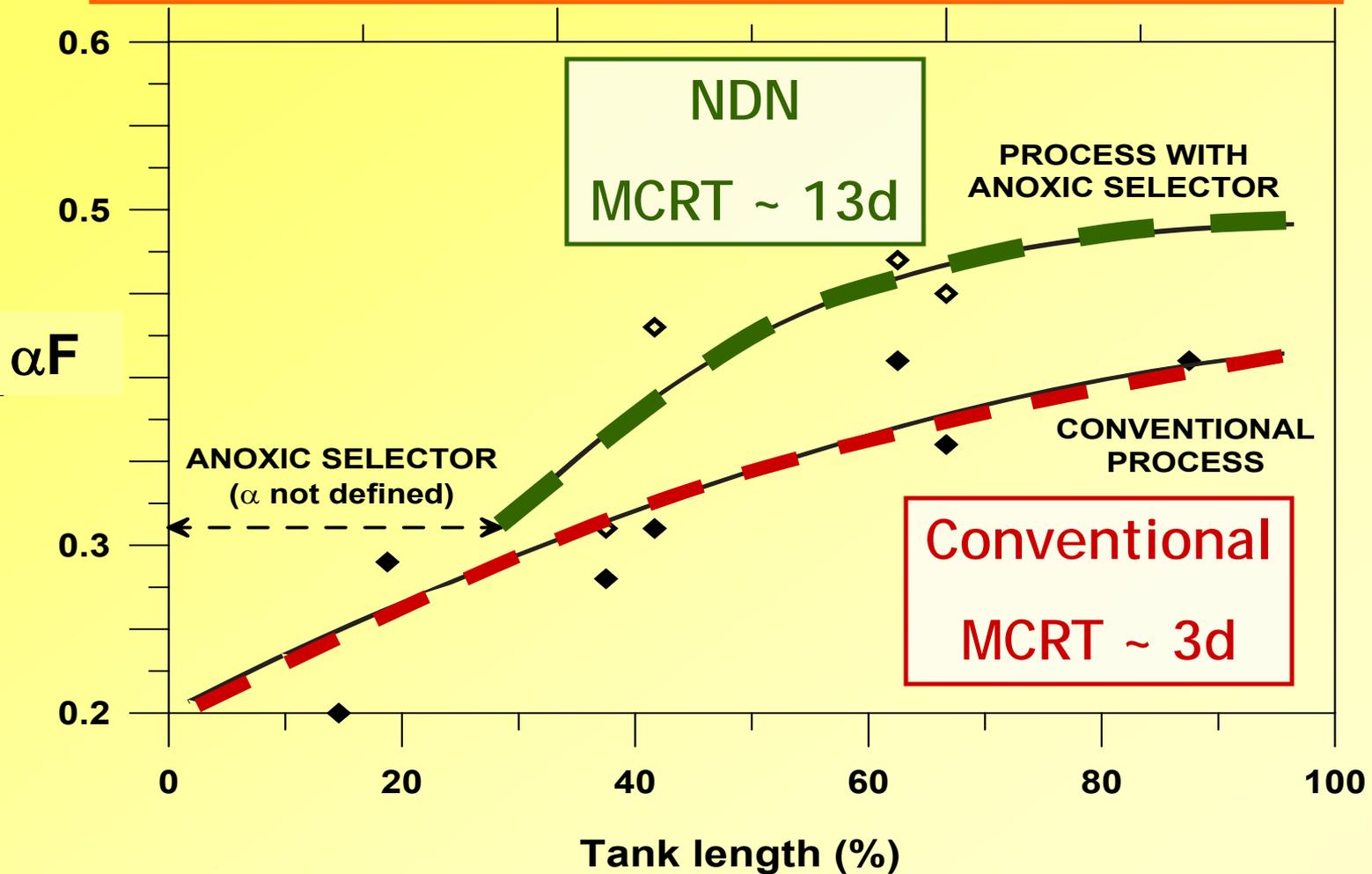


NDN LAYOUT



Alpha: Conventional vs. NDN

AERATION ENERGY $\sim 1/\alpha F$





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II. MEASUREMENT OF OXYGEN TRANSFER IN CLEAN WATER

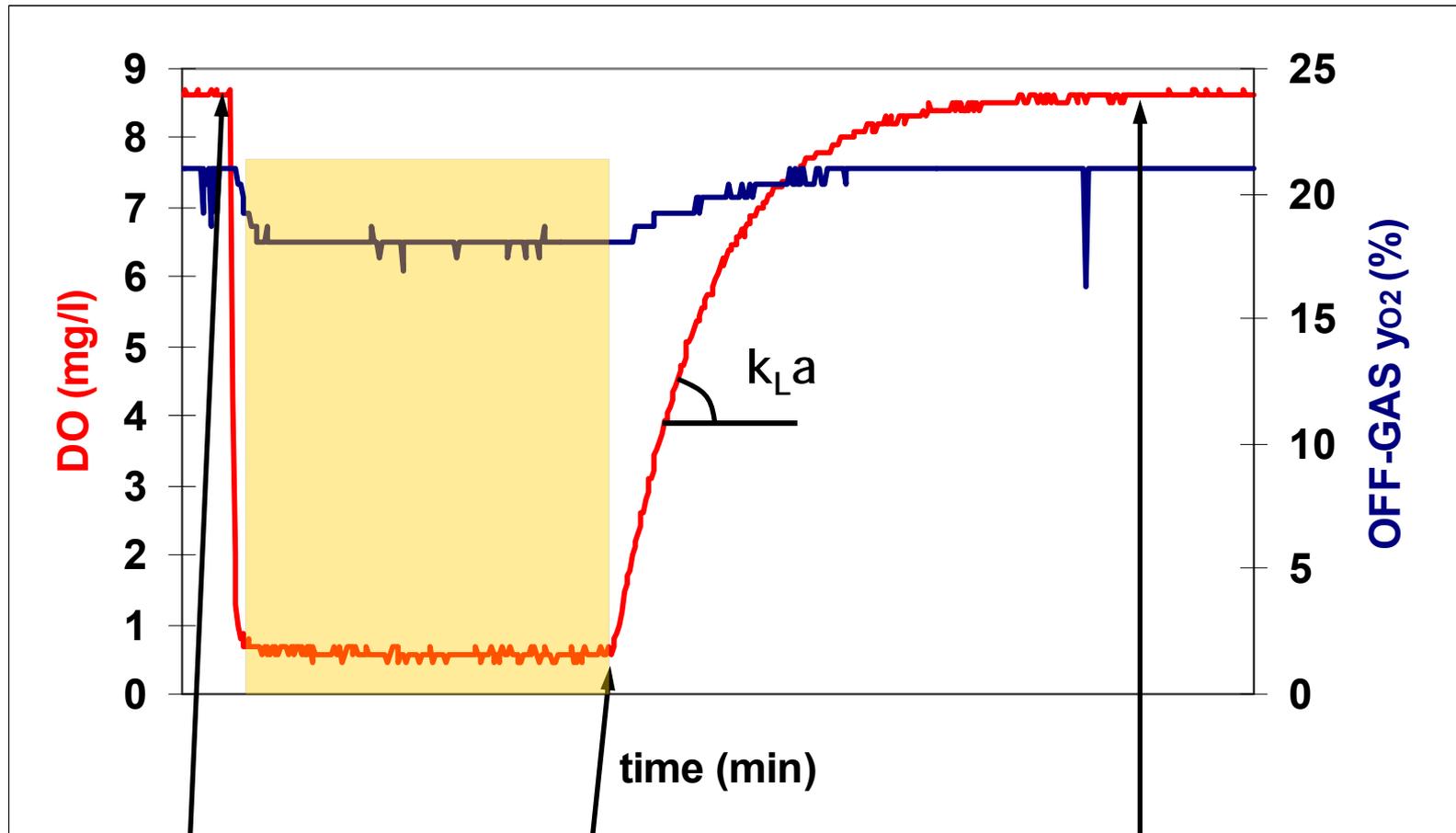
Lab-scale aeration tank



Dimensions: 3 x 3 x 5 ft
Submergence: 4 ft



Clean Water Test results



Na₂SO₃ added

O₂ scavenging completed

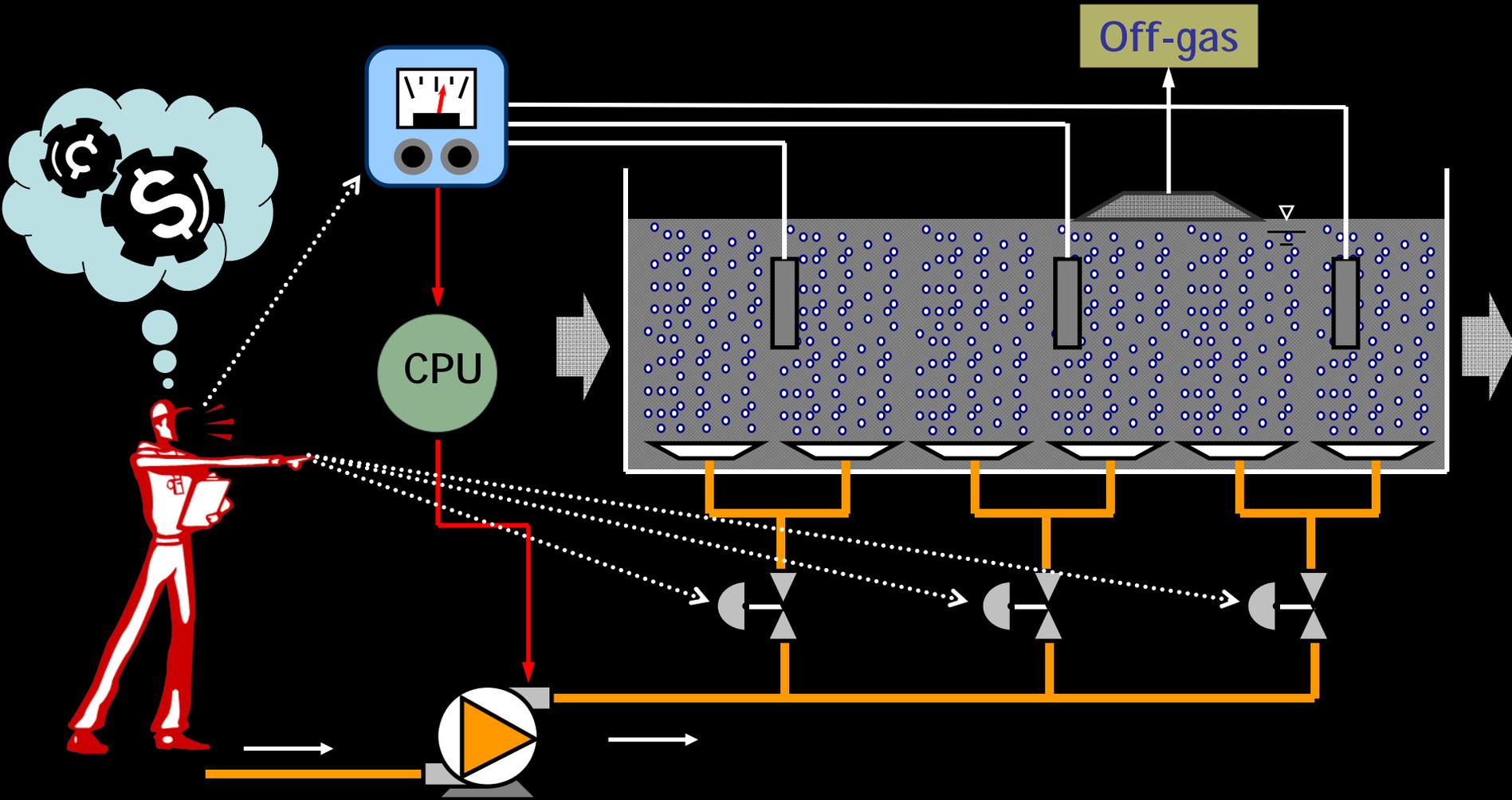
C_{sat} is reached



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III. FIELD MEASUREMENTS OF OXYGEN TRANSFER IN WASTEWATER

AERATION EFFICIENCY TESTING



$$\text{OTR} = (k_L a \cdot V) [C_{\text{sat}} - (\text{DO}_{\text{exc}} + \text{DO}_{\text{needed}})] = \text{kg}_{\text{O}_2}/\text{d} = \text{\$/d}$$

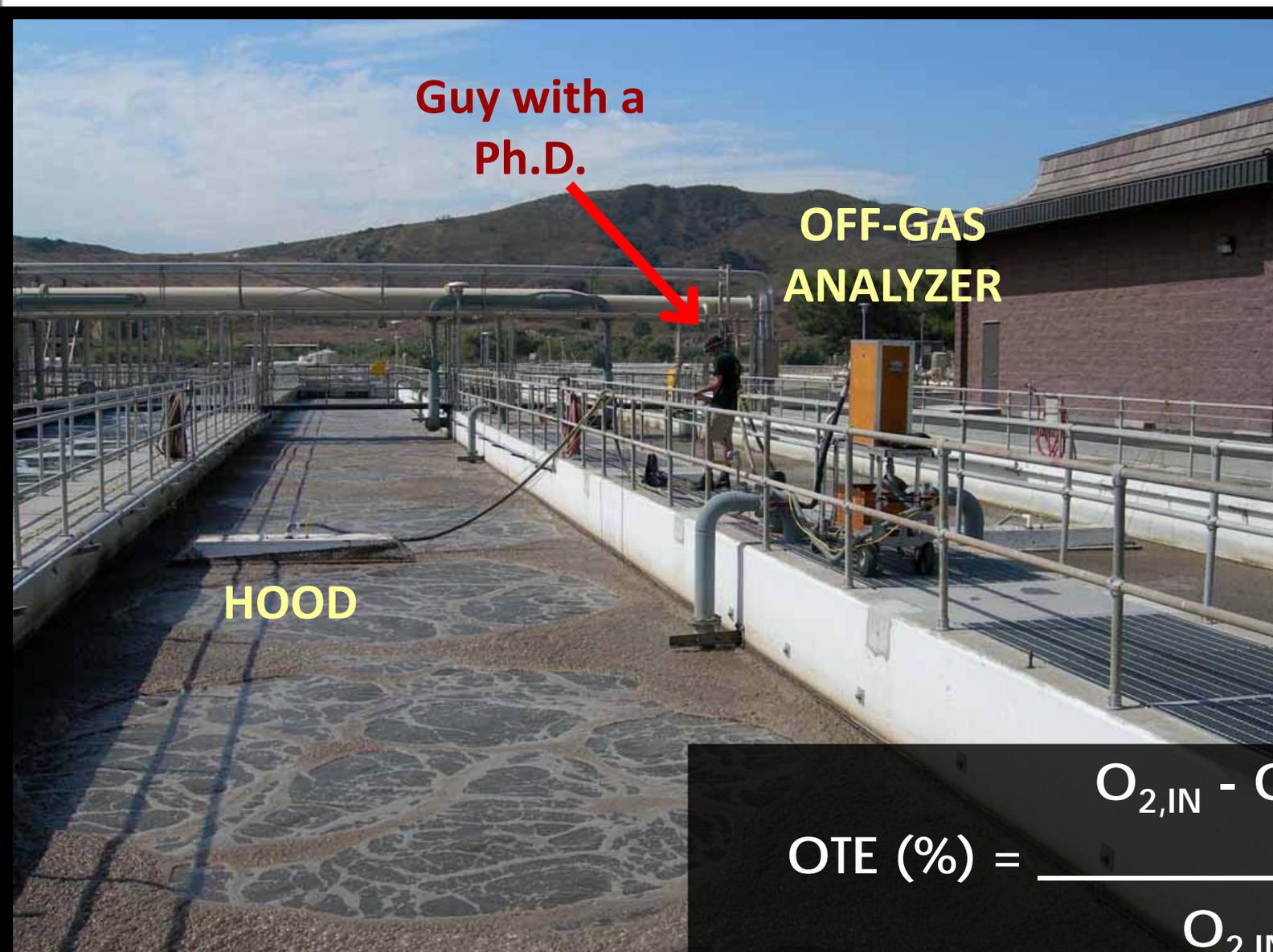
TRADITIONAL OFF-GAS TESTING SETUP

Guy with a
Ph.D.

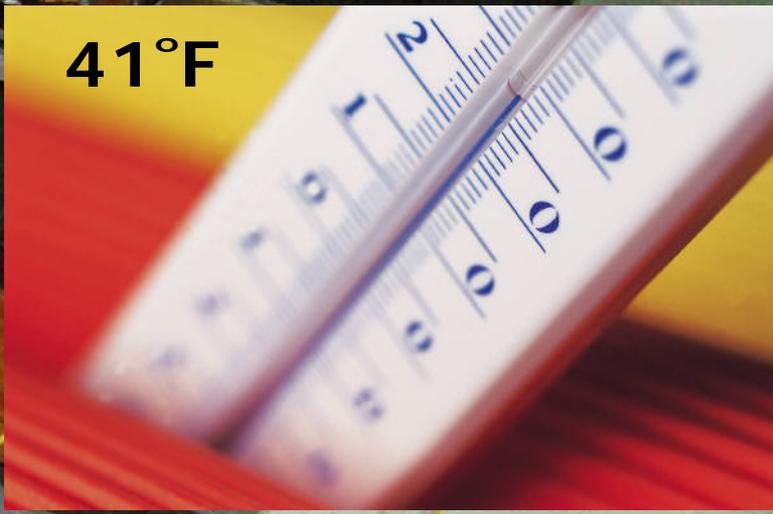
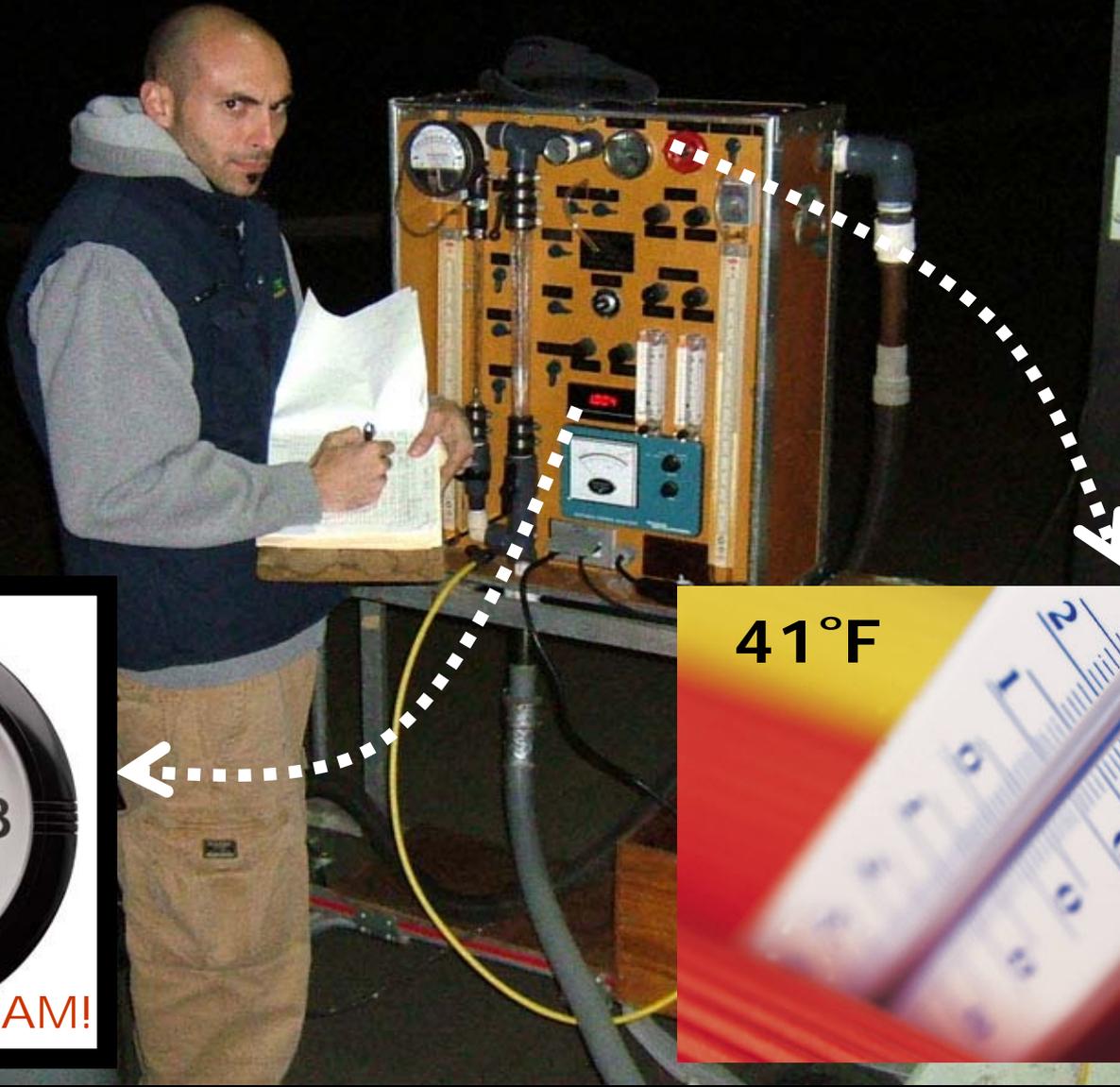
OFF-GAS
ANALYZER

HOOD

$$\text{OTE (\%)} = \frac{\text{O}_{2,\text{IN}} - \text{O}_{2,\text{OUT}}}{\text{O}_{2,\text{IN}}}$$



PITFALLS OF TESTING...



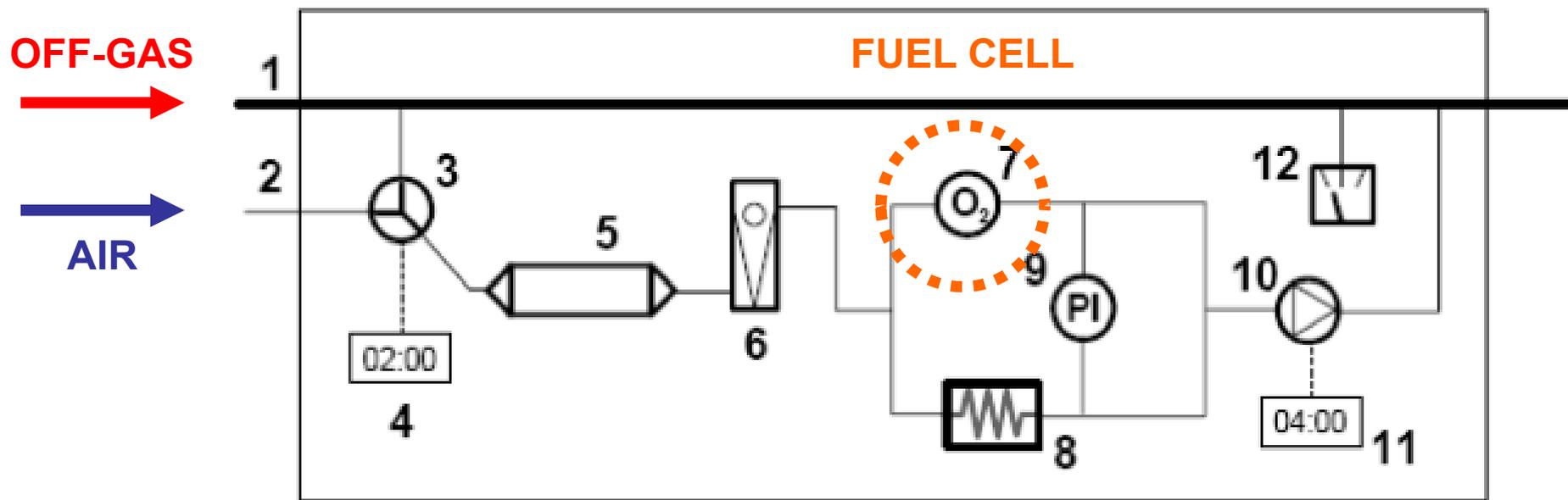
CURRENT OFF-GAS SETUP

AUTOMATED
ANALYZER

MANUAL
ANALYZER



Schematic of automated analyzer

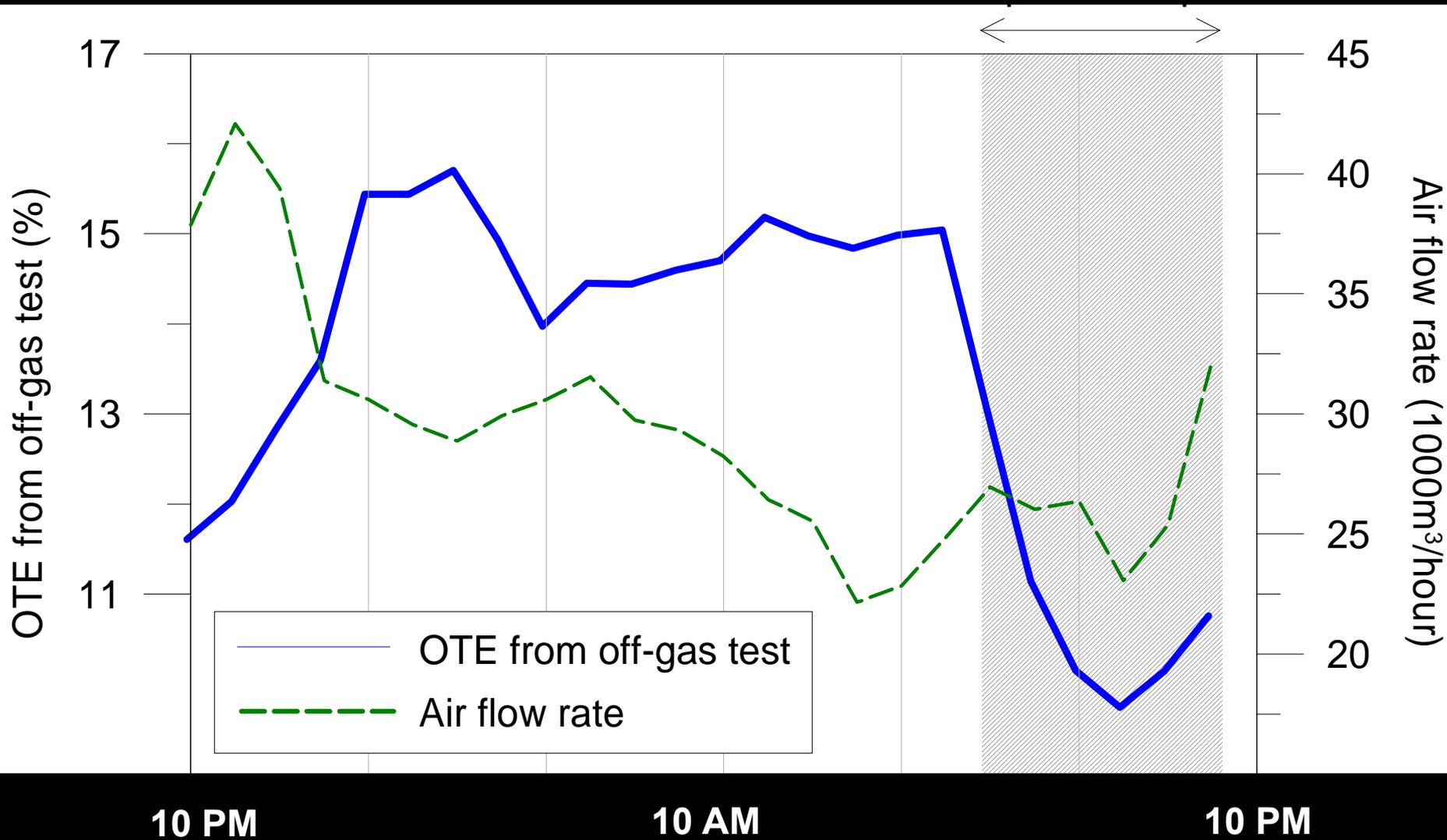


Key: 1) off-gas hose (from collection hood); 2) reference air intake; 3) three-way valve; 4) time delay relay; 5) column for CO_2 and H_2O removal; 6) flow meter; 7) oxygen fuel cell; 8) resistance; 9) differential manometer; 10) vacuum pump; 11) time delay relay; 12) air velocity meter. Solid lines = hydraulic line, dashed lines = electrical connection

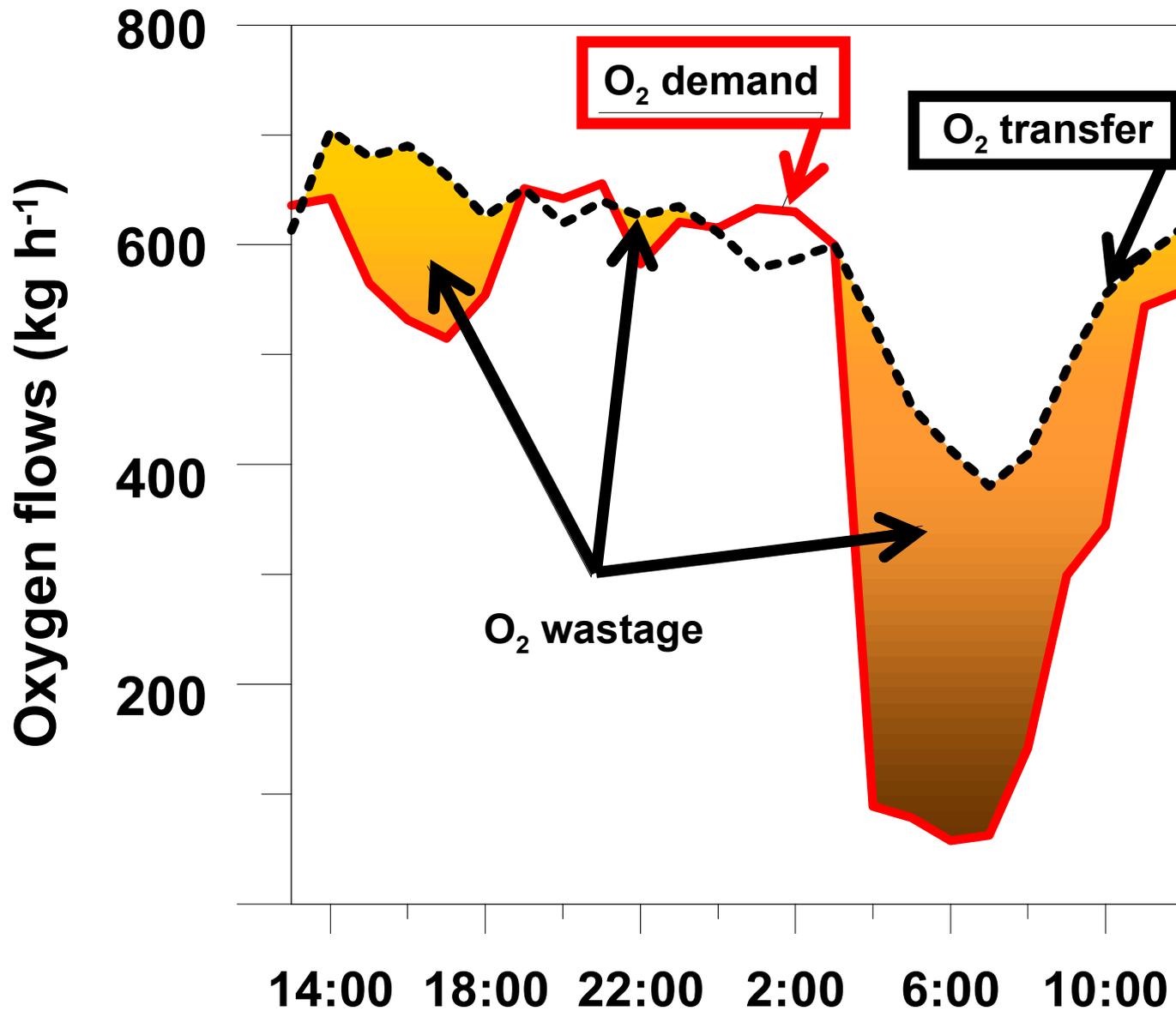
REAL-TIME OFF-GAS ANALYSIS



24hr MONITORING



24 hrs – PLANT OPERATIONS

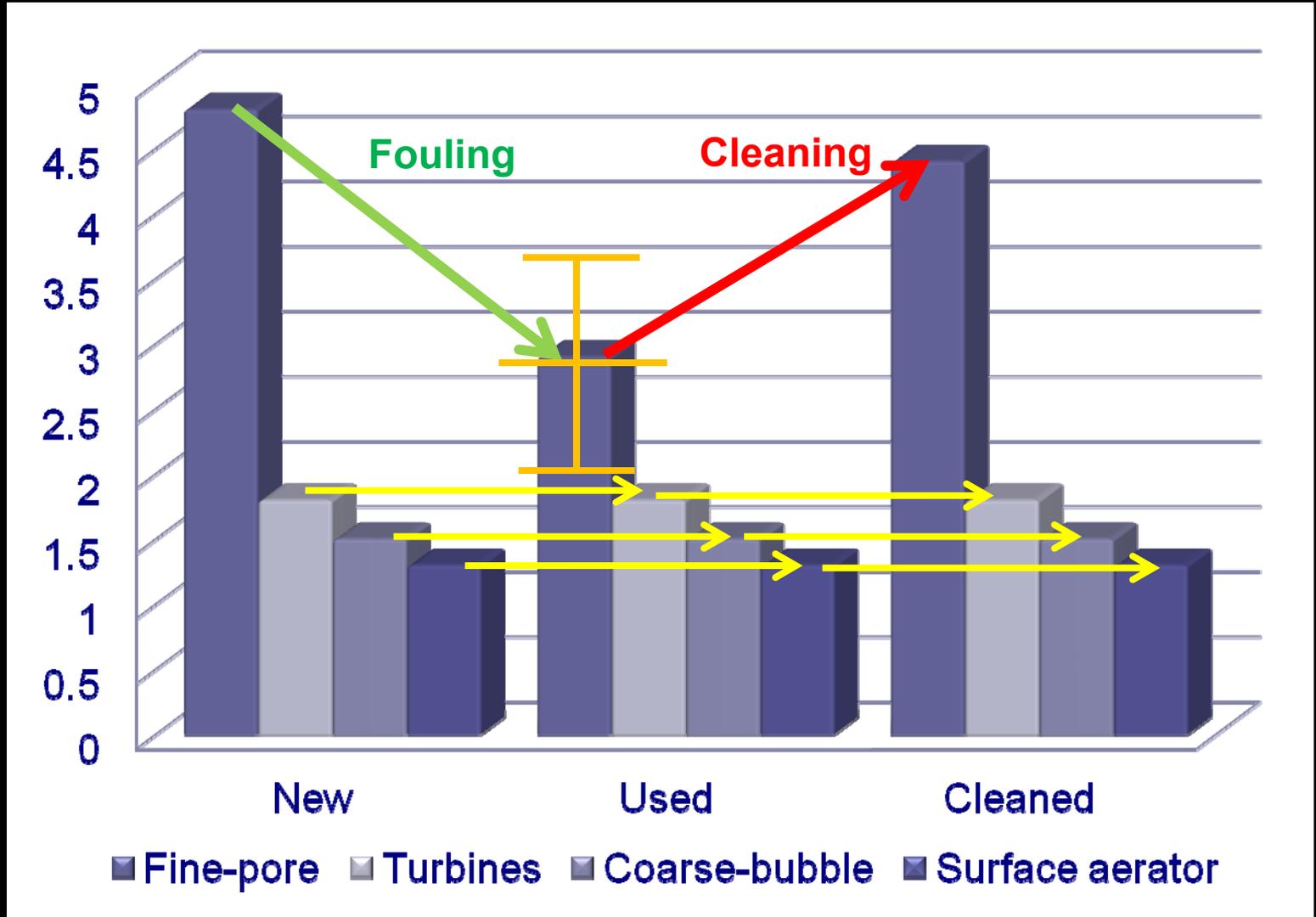




IV. LONG-TERM DIFFUSER FOULING

Aeration Efficiency over time

STANDARD AERATION EFFICIENCY
(kg O₂ / kWh)



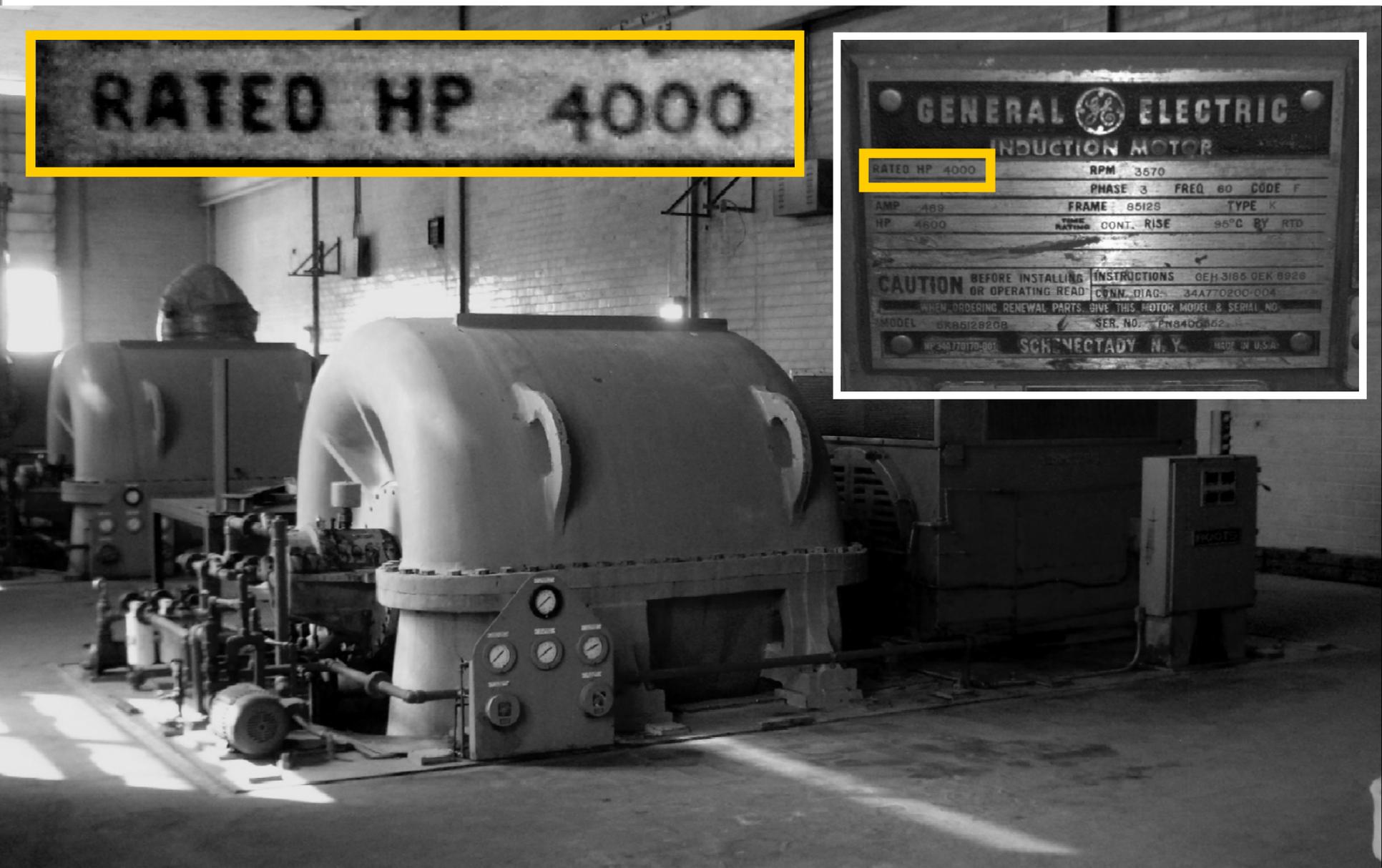
Big challenges

RATED HP 4000

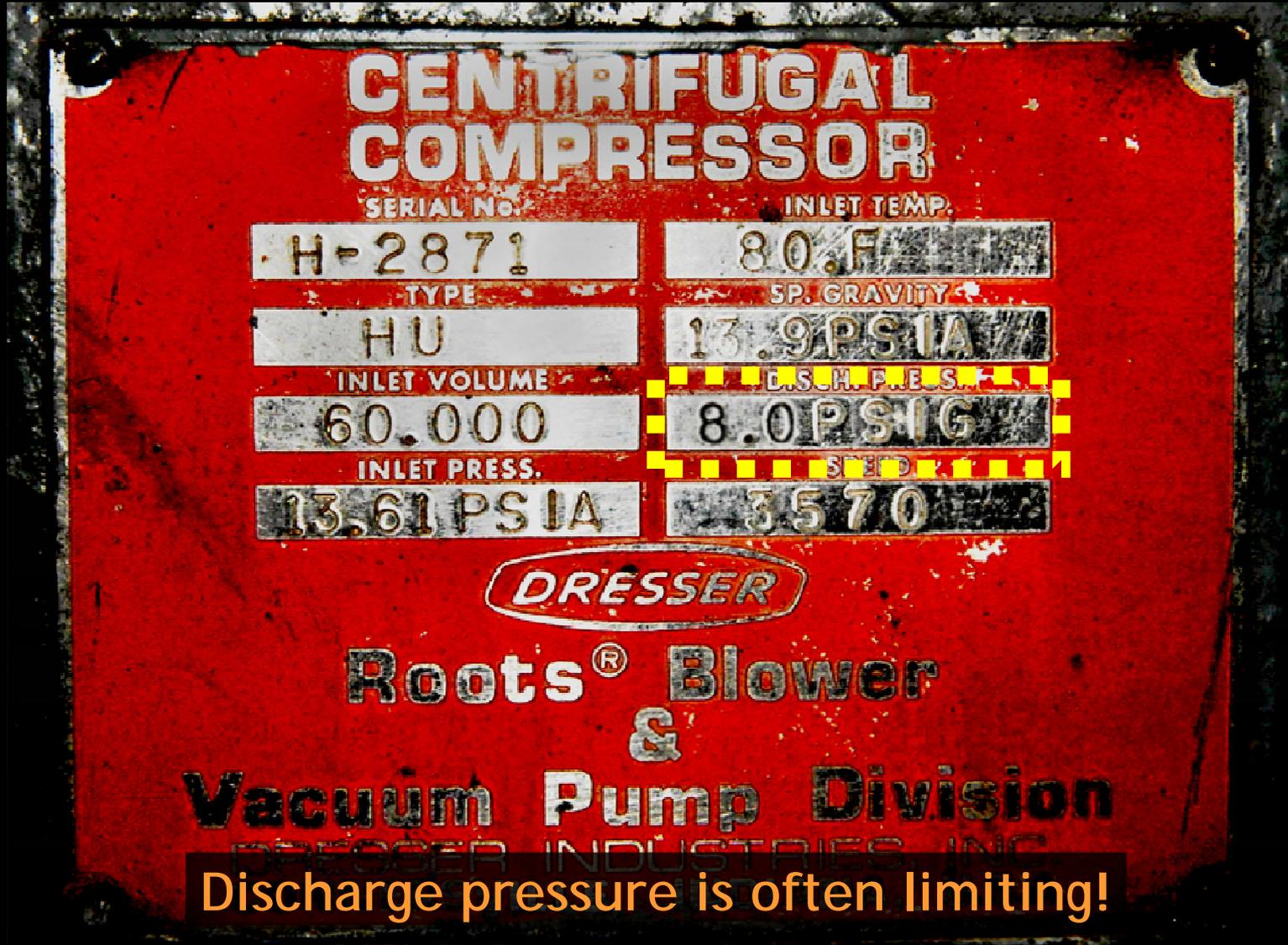
GENERAL ELECTRIC
INDUCTION MOTOR

RATED HP 4000	RPM 3570
AMP 469	PHASE 3 FREQ 60 CODE F
HP 4600	FRAME 8512S TYPE K
	TIME RATING CONT. RISE 95°C BY RTD

CAUTION BEFORE INSTALLING OR OPERATING READ INSTRUCTIONS GEH 3185 GEK 8926
WHEN ORDERING RENEWAL PARTS, GIVE THIS MOTOR MODEL & SERIAL NO.
CONN. DIAG. 34A770200-004
MODEL 6R8512820B SER. NO. 47B8400362
SCHENECTADY N. Y. MADE IN U.S.A.



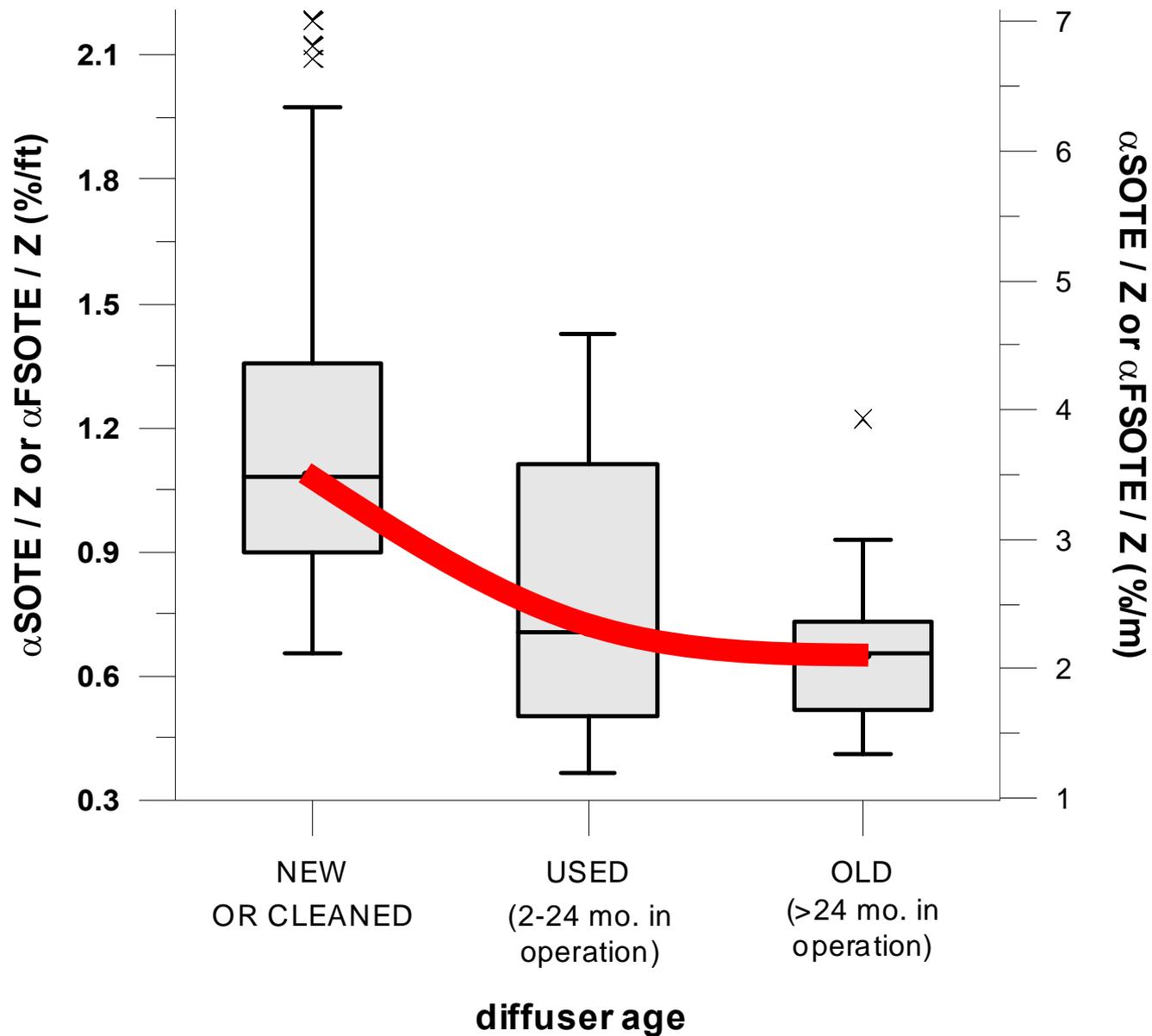
Blower limits



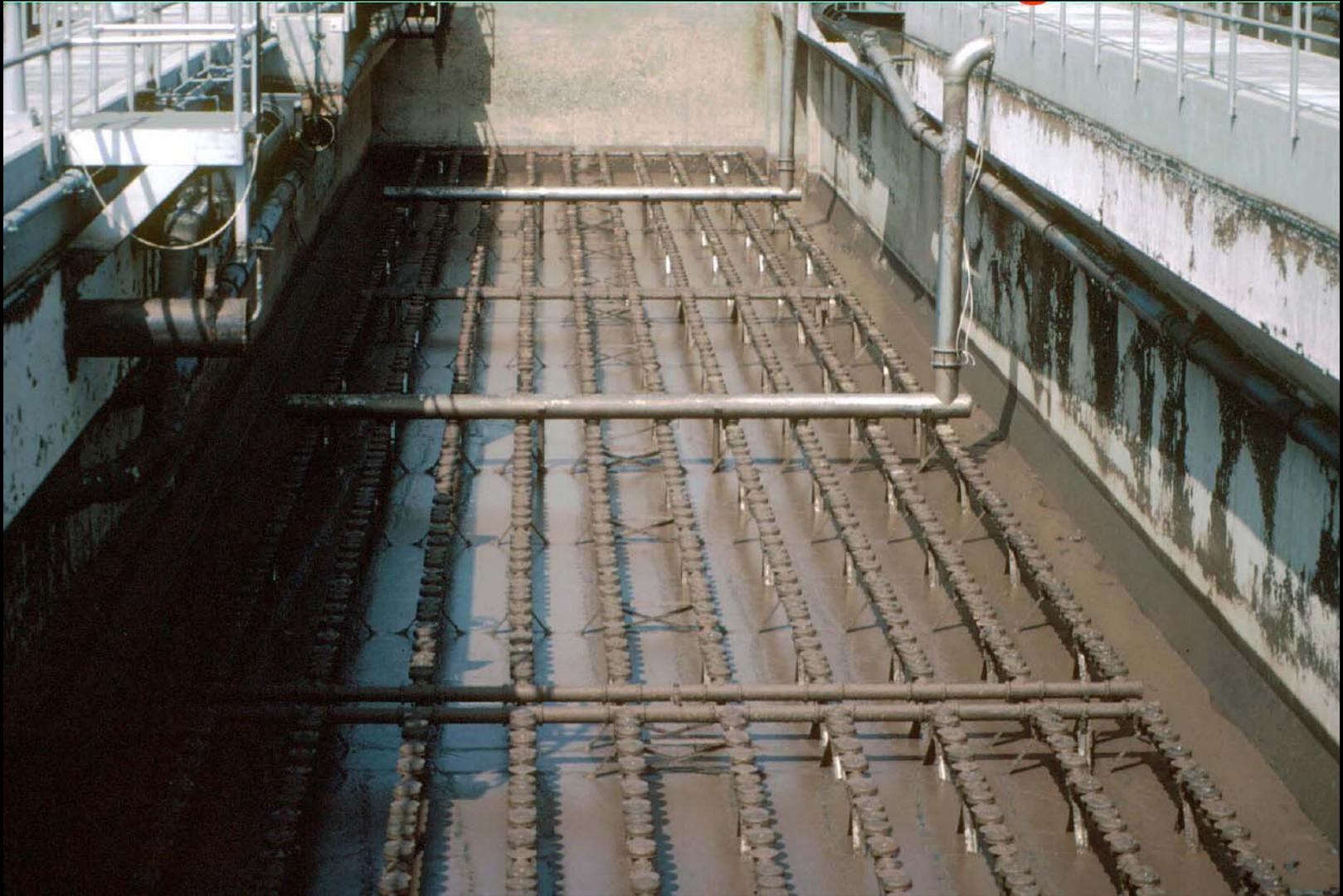
Blowers rule

**BLOWERS DO NOT COMPRESS AIR,
THEY BLOW IT.**

Plant histories of efficiency: \langle SOTE



Pre-cleaning



Post-cleaning



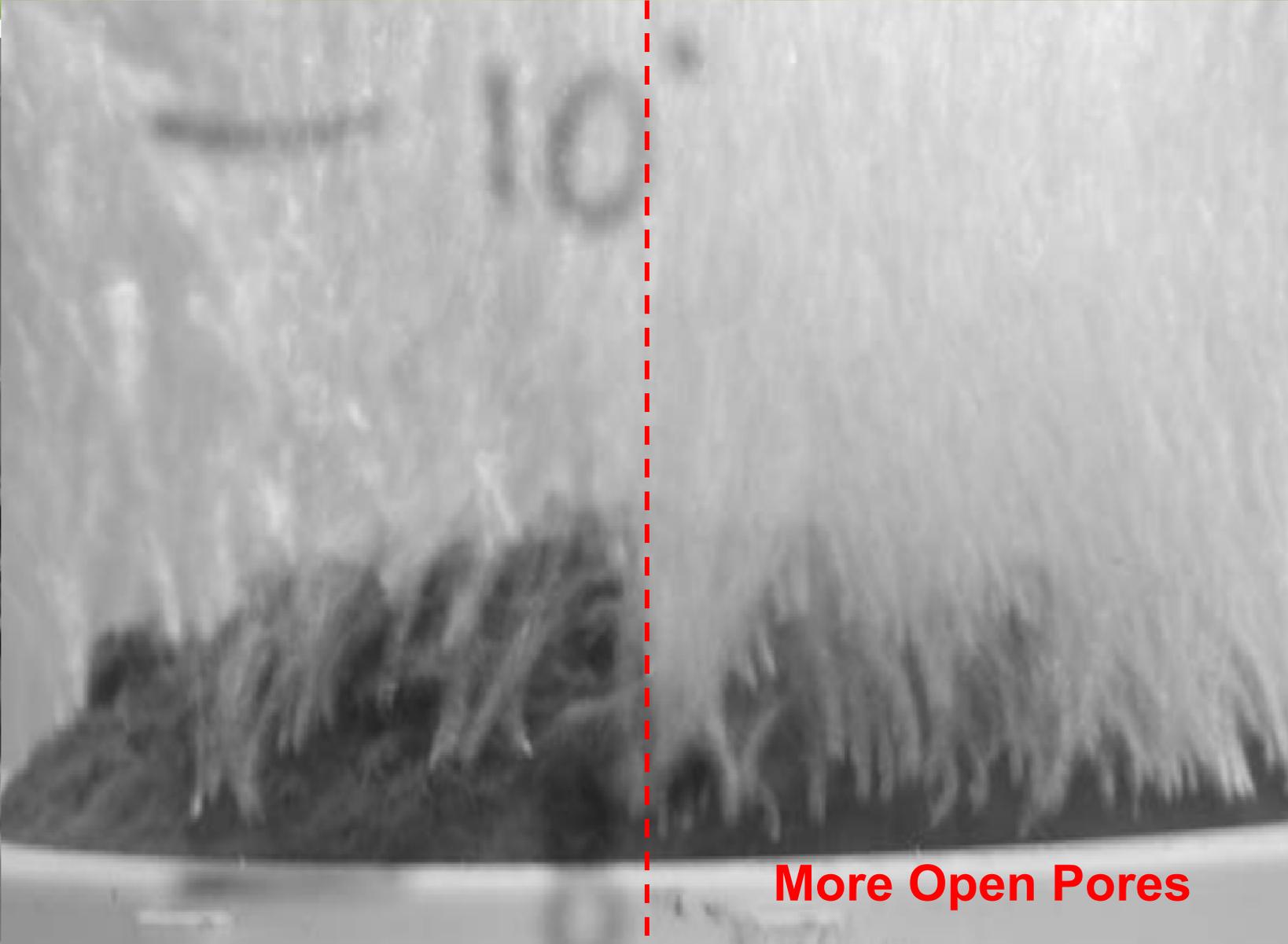
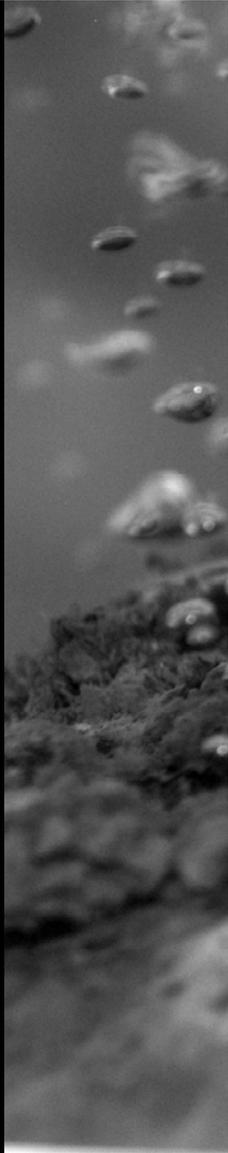
Half & Half



FOULED

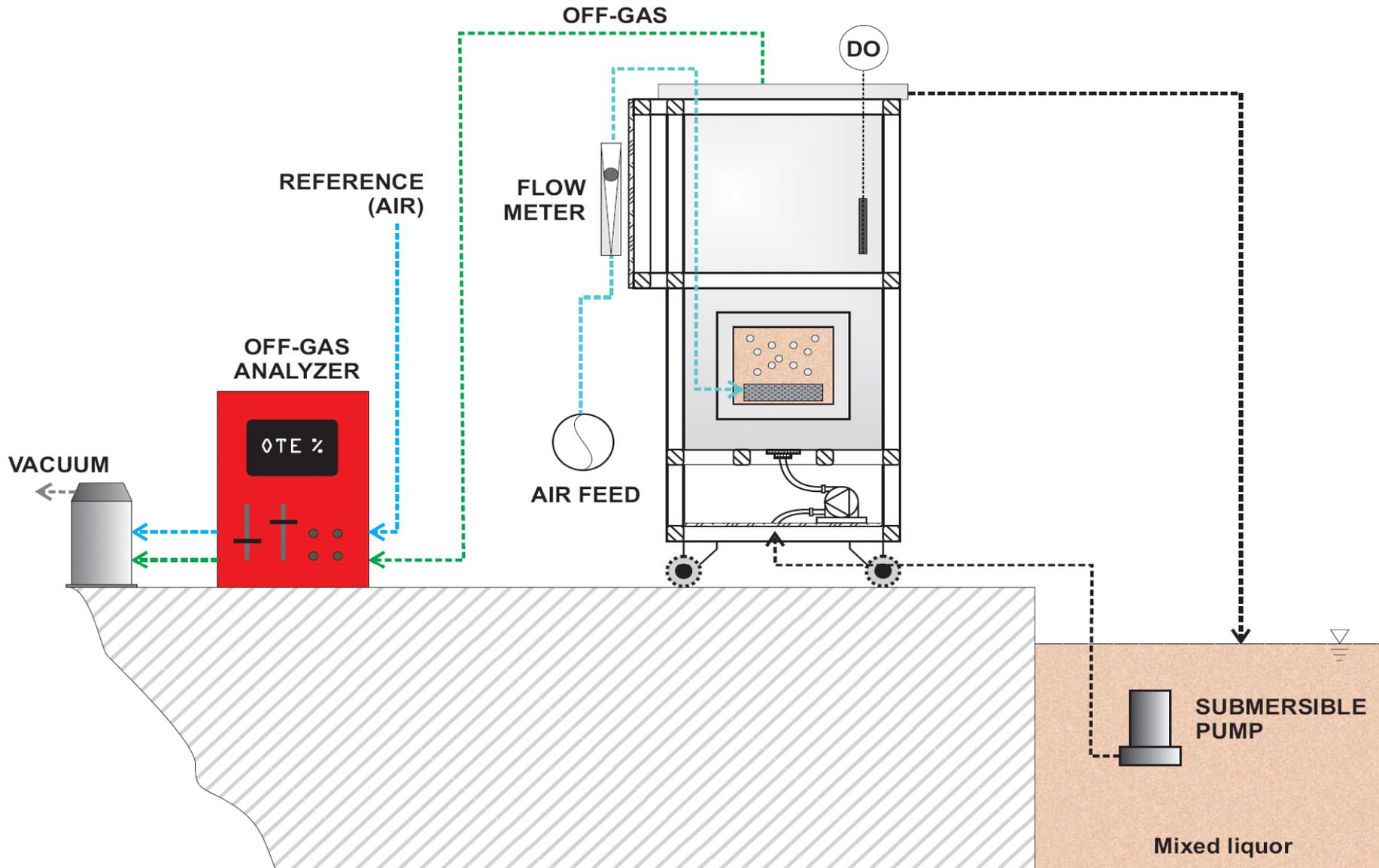
CLEANED

Bubble release at operating regime

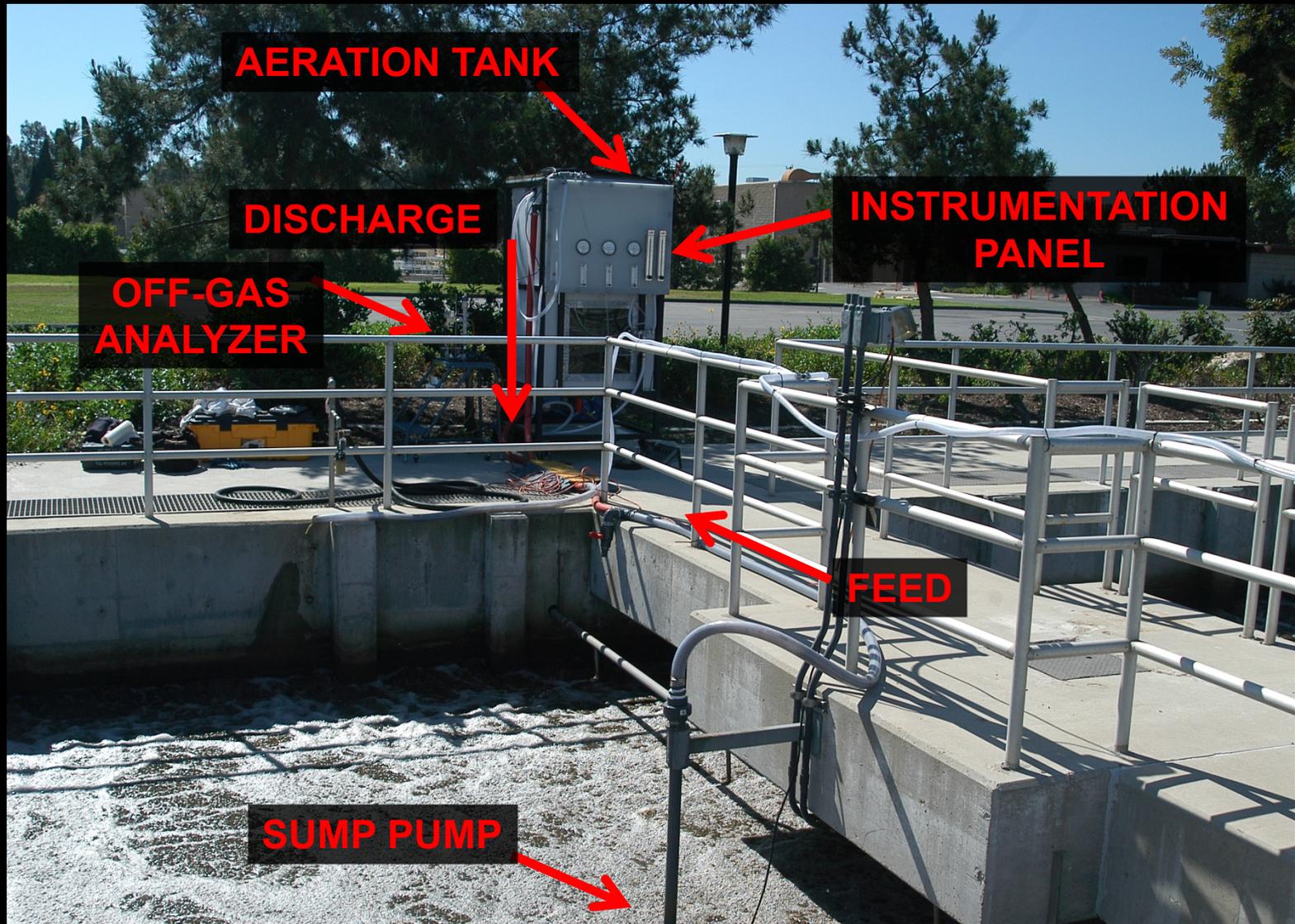


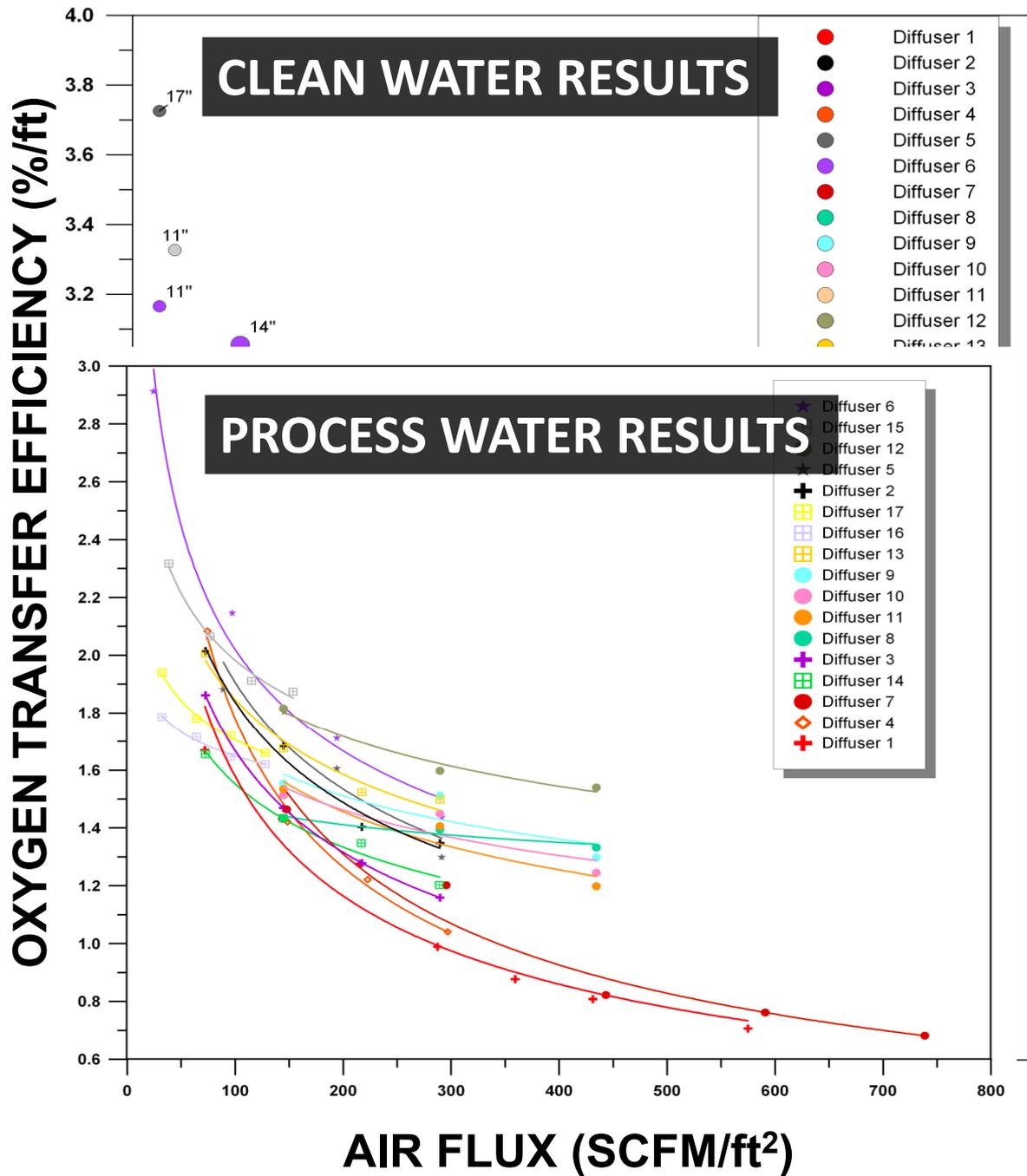
More Open Pores

ON-SITE COLUMN TESTING IN WWTPs

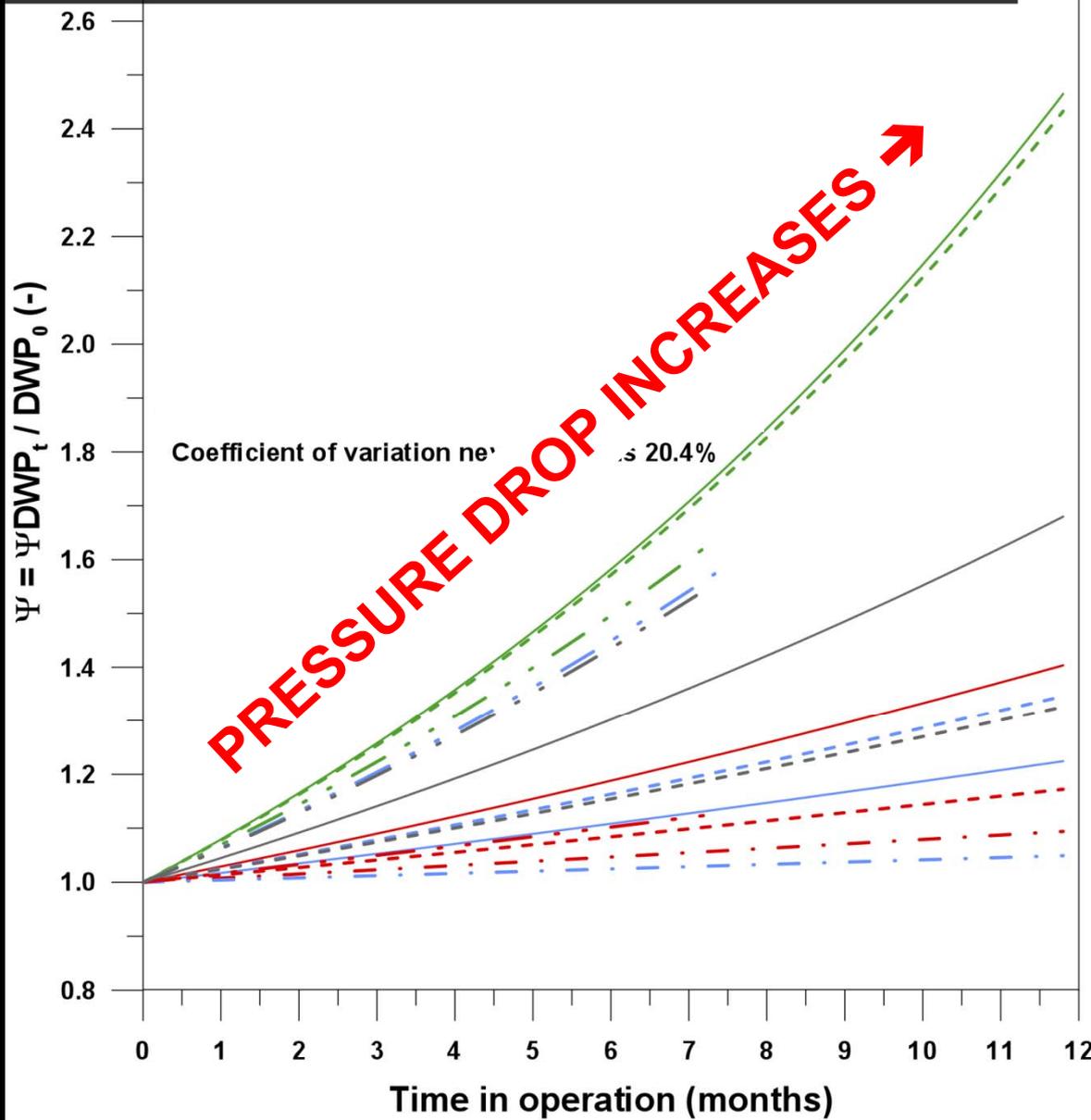
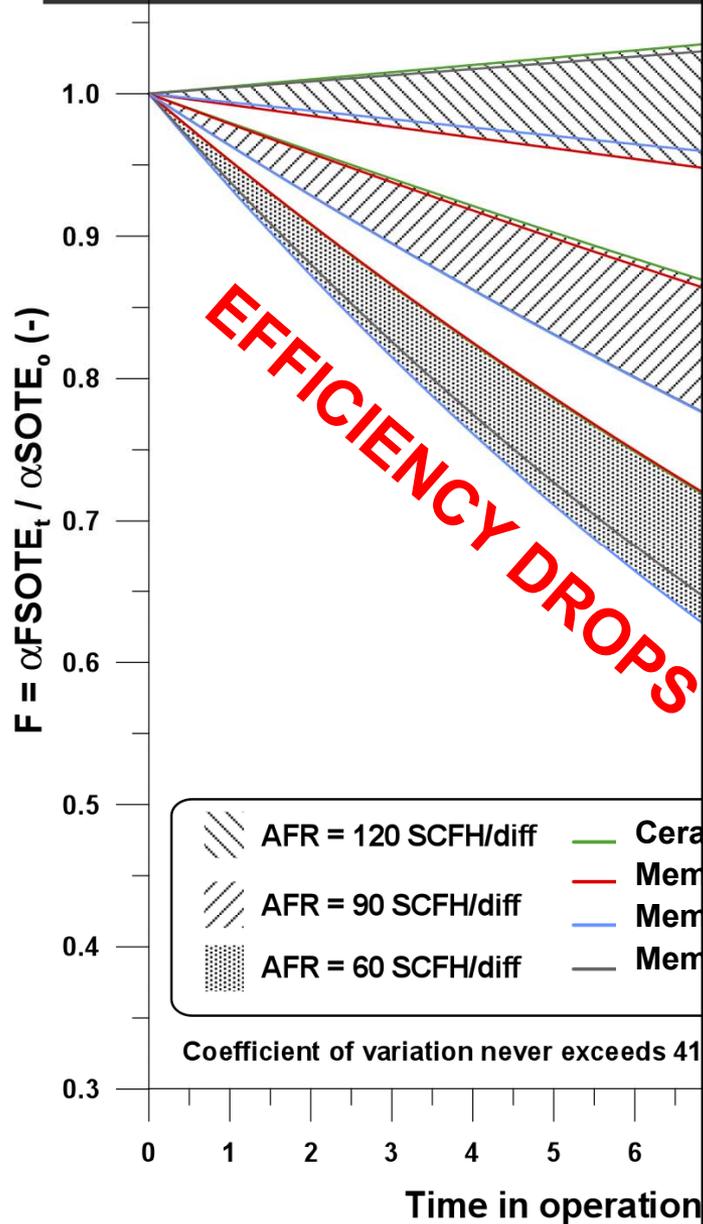


Bridging Present and Future : Fouling Studies





FOULING & PRESSURE DROP RESULTS



Fine-pore diffusers: clean them or don't buy them





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V. LABORATORY DIFFUSER TESTING

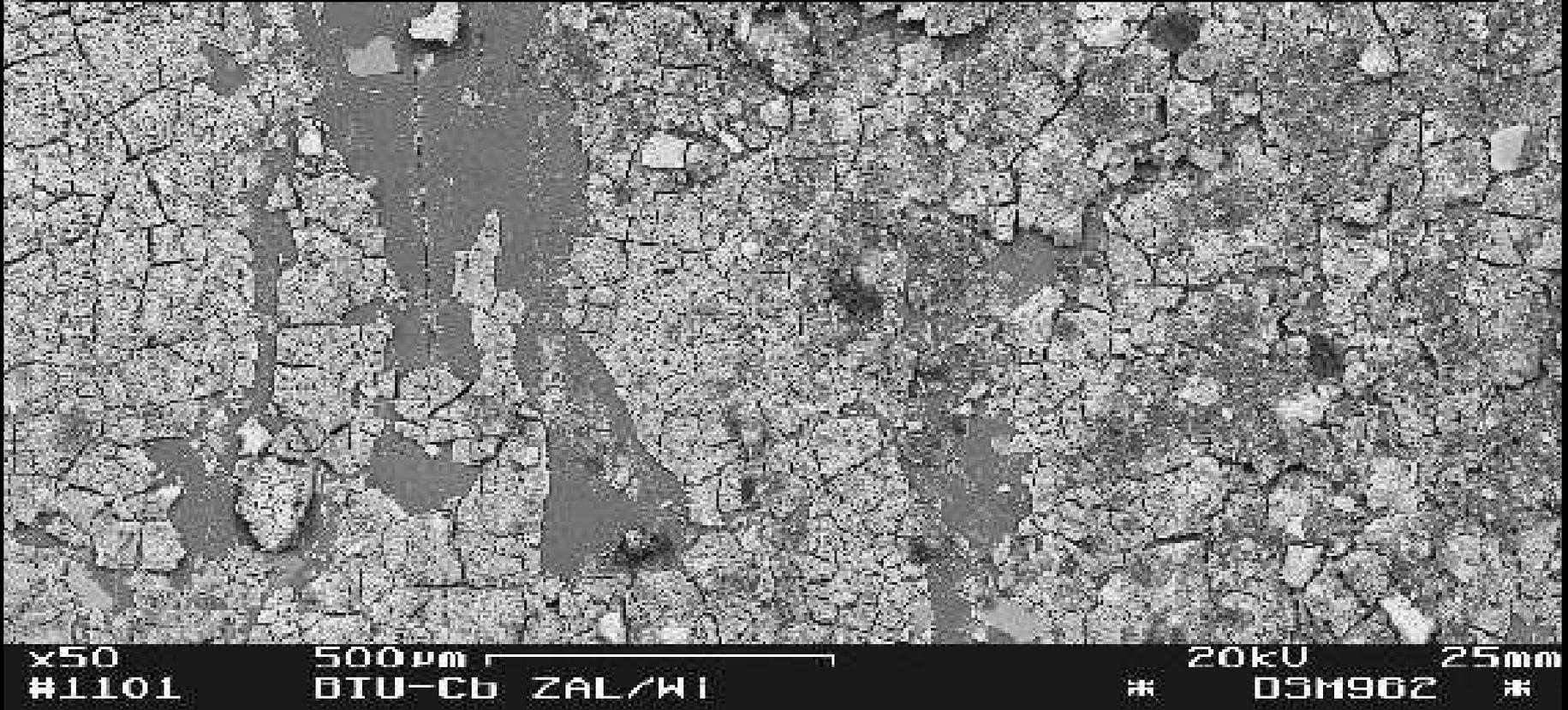
Optical Microscopy

- Suitable for imaging orifice dimensions and geometry
- Rapid and not labor-intensive
- HD cameras used
- Suitable to test diffusers while operating on bench-top mounts at variable air flows
- Example of a silicone membrane pore →

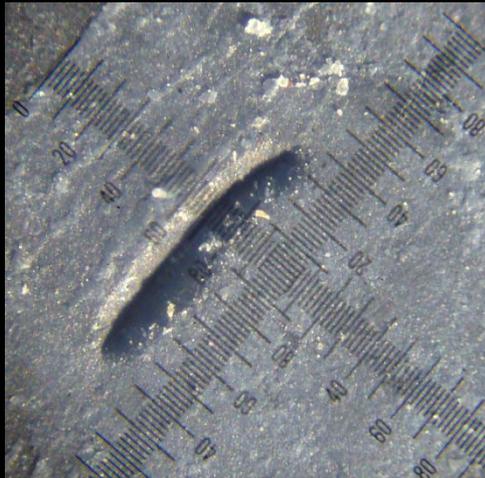


Electron Microscopy

Example of using electronic microscopy to characterize surface deposits onto membrane diffusers. This was a silicone diffuser membrane in an industrial treatment plant, showing a combination of inorganic scales and biological fouling (Rosso et al, 2008).



Optical evidence of orifice clogging



New

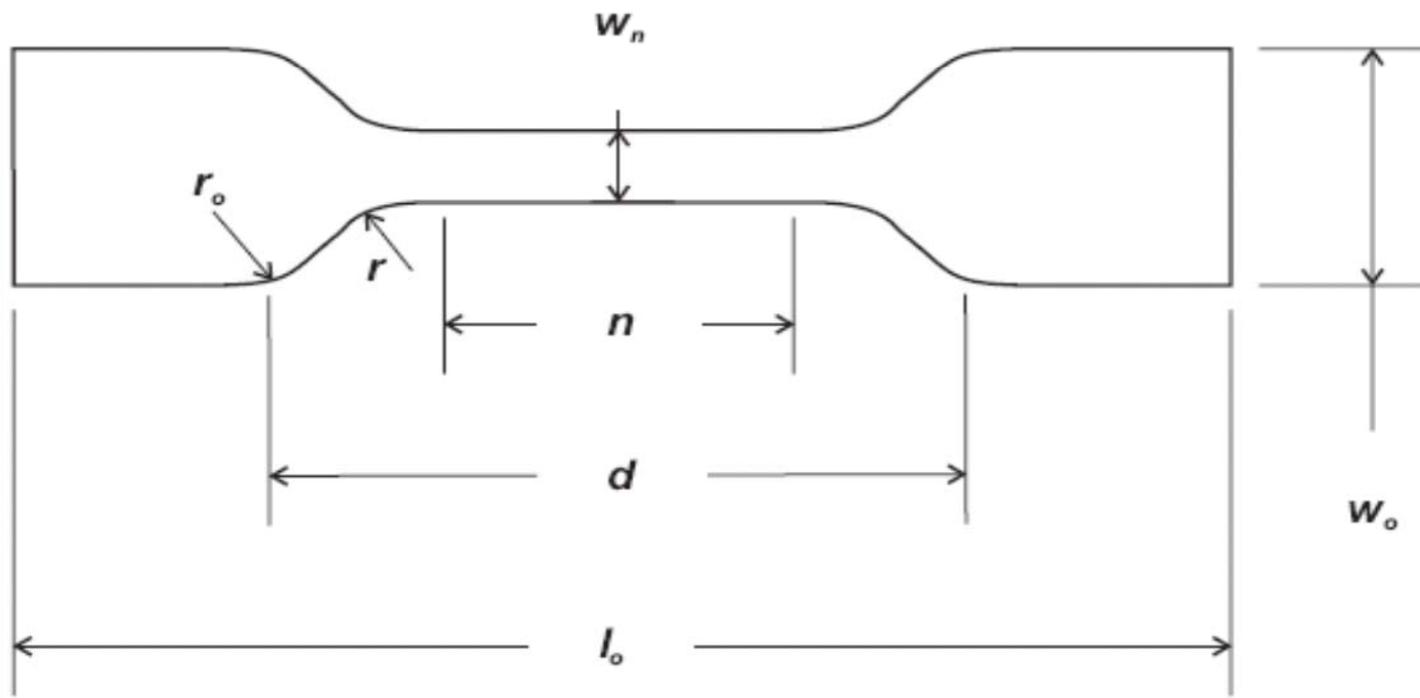
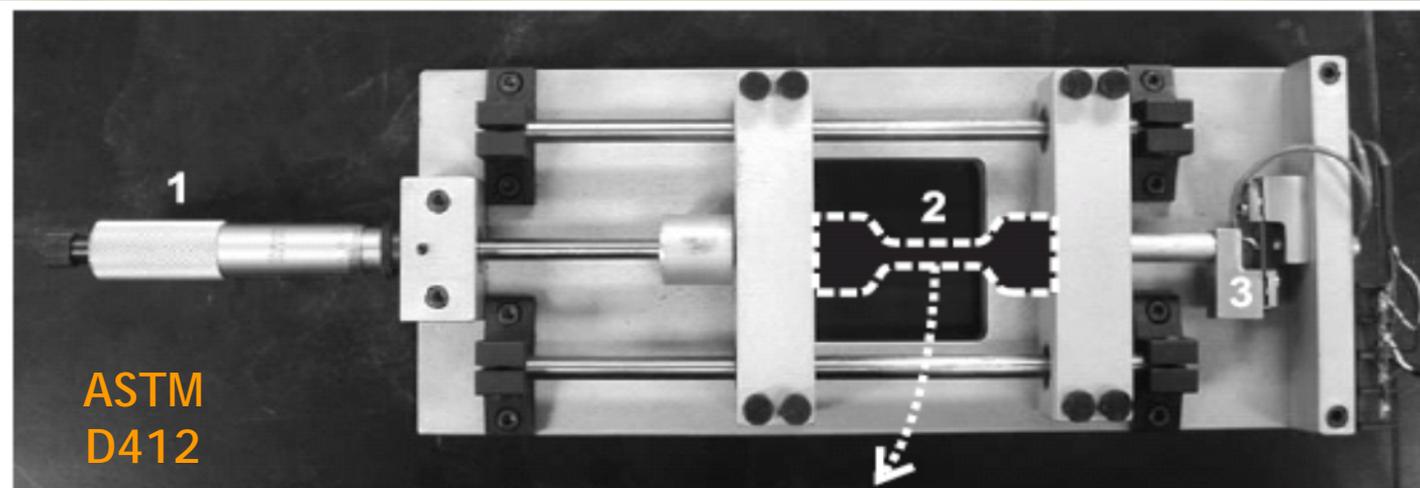


Fouled



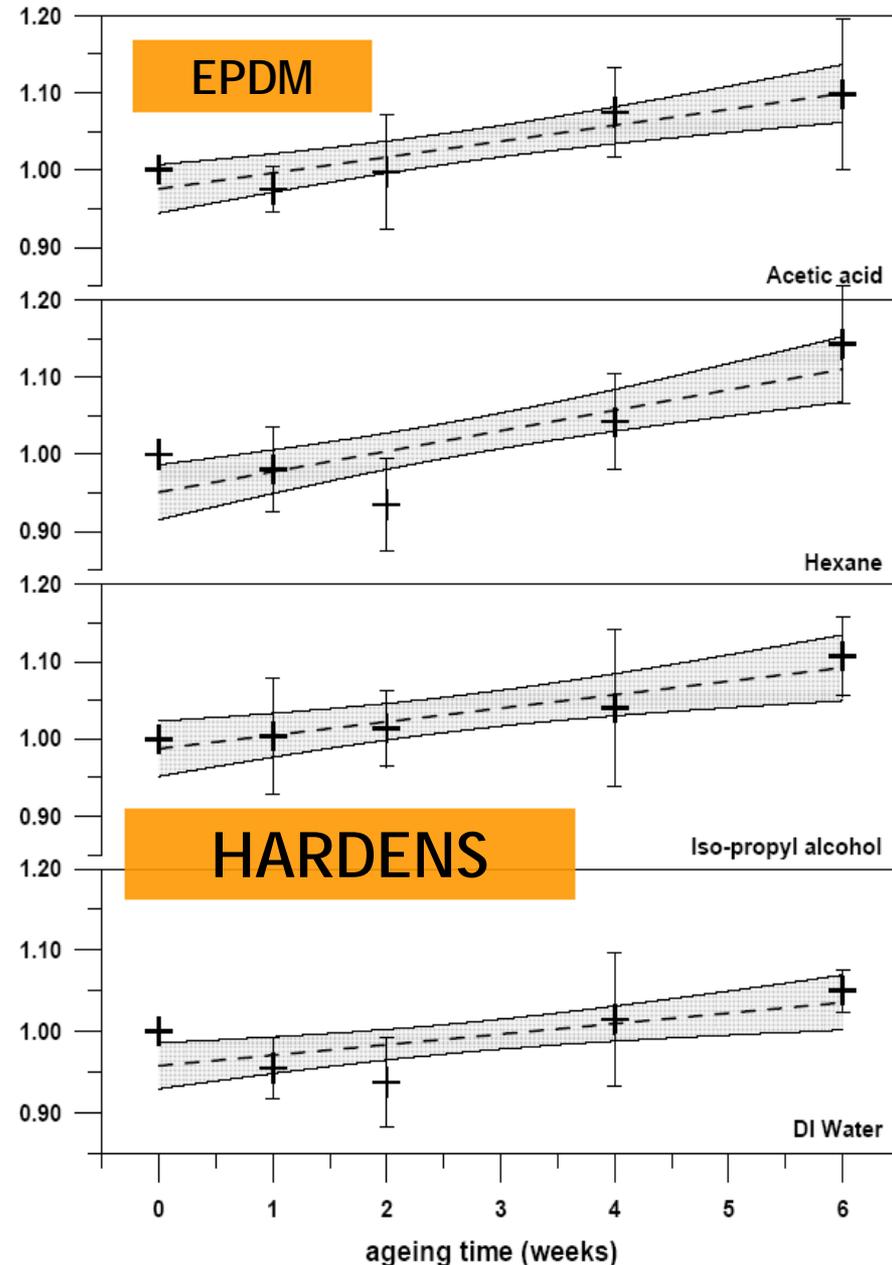
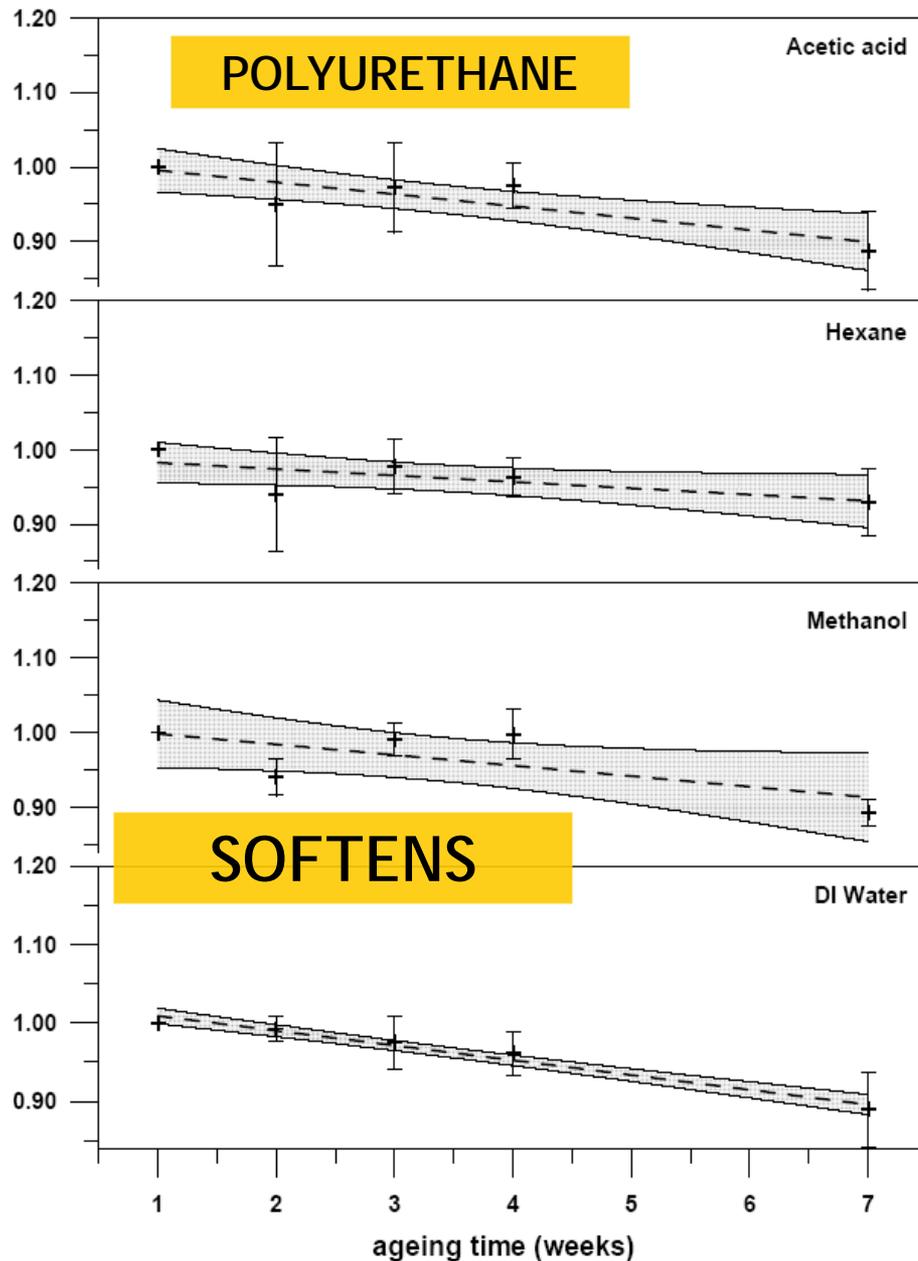
Cleaned

Loading Cell – Stress vs. Strain



YOUNG'S MODULUS

Normalized Young's modulus of elasticity

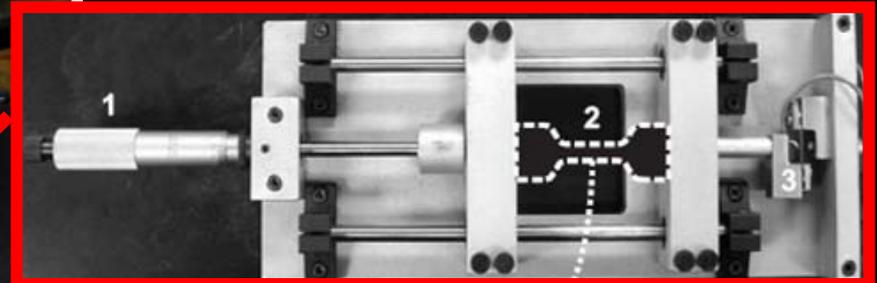
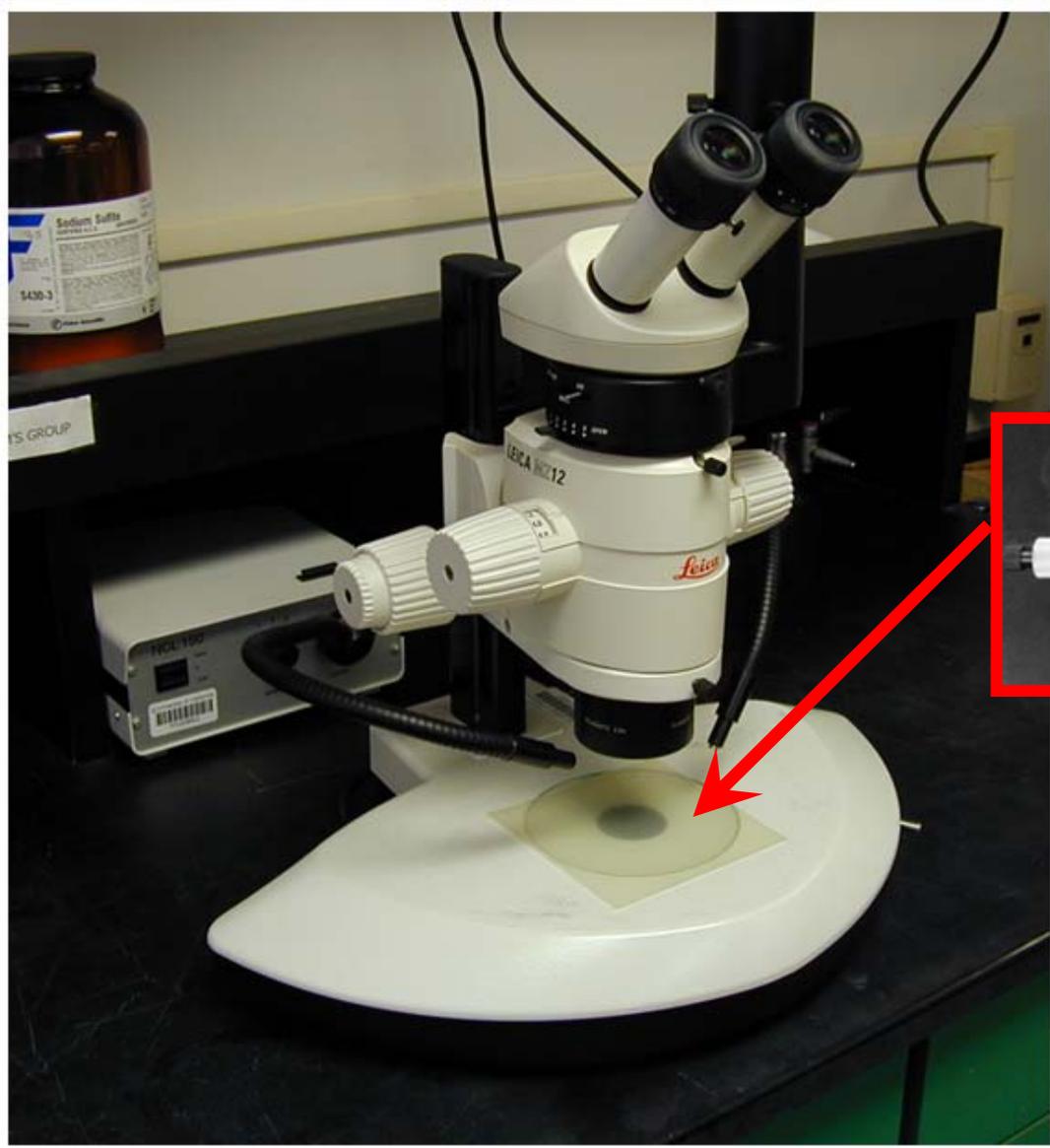


Thickness

- Micrometric measurements for thickness
- Pressure-sensitive micrometer used
- 10 membrane points sampled
- 4-8 fold membrane thicknesses



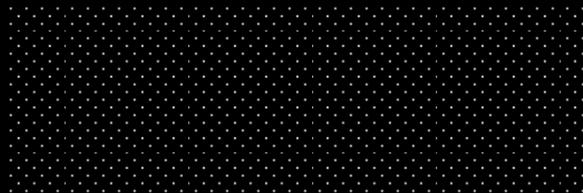
ORIFICE CREEP TESTS



DUROMETRIC TESTS



**SHORE A
HARDNESS**



MEMBRANE SAMPLE

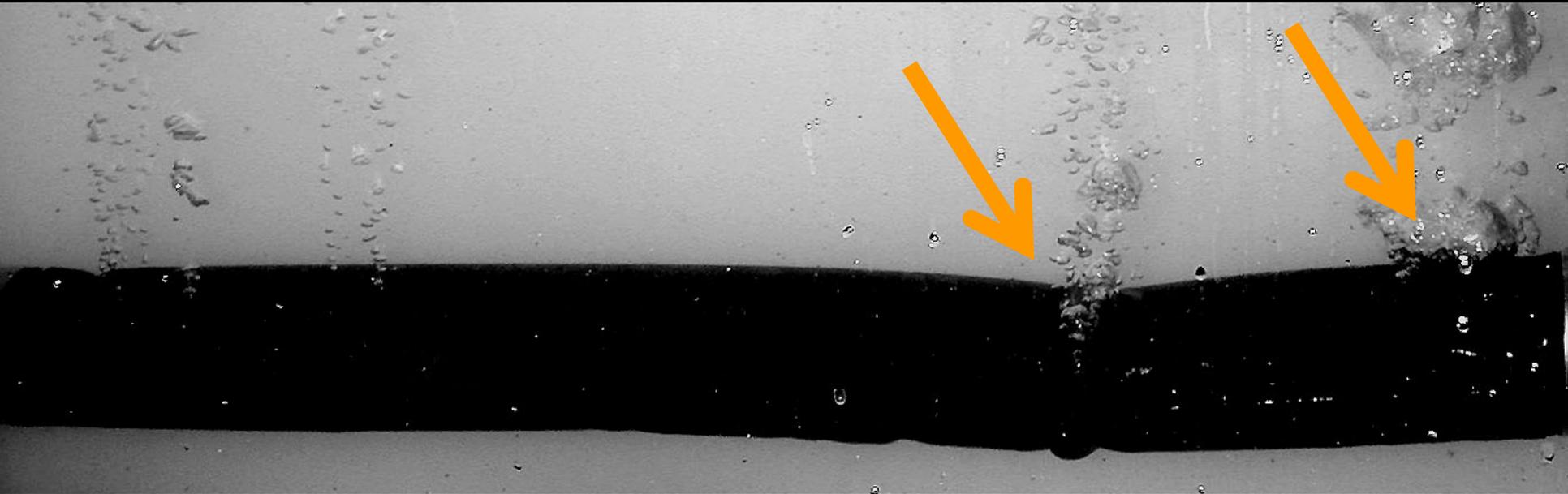


HALF & HALF



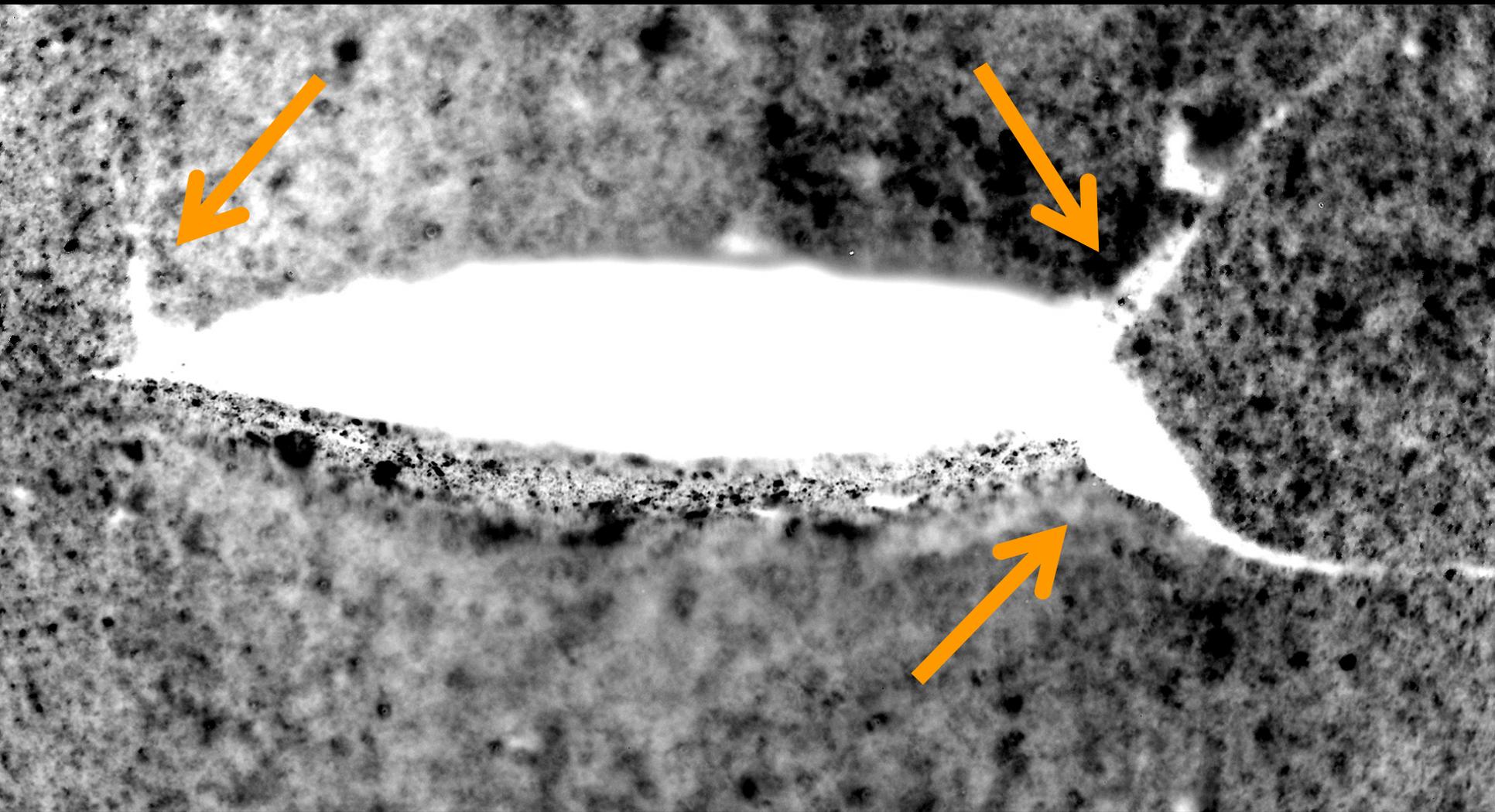
- Orifice creep caused sludge to enter the diffuser and form a crust inside

CRACKS IN FOLD



- Membrane sheath typically longer than frame
- To compensate for shrinkage
- Folds are formed

CRACKS IN FOLD

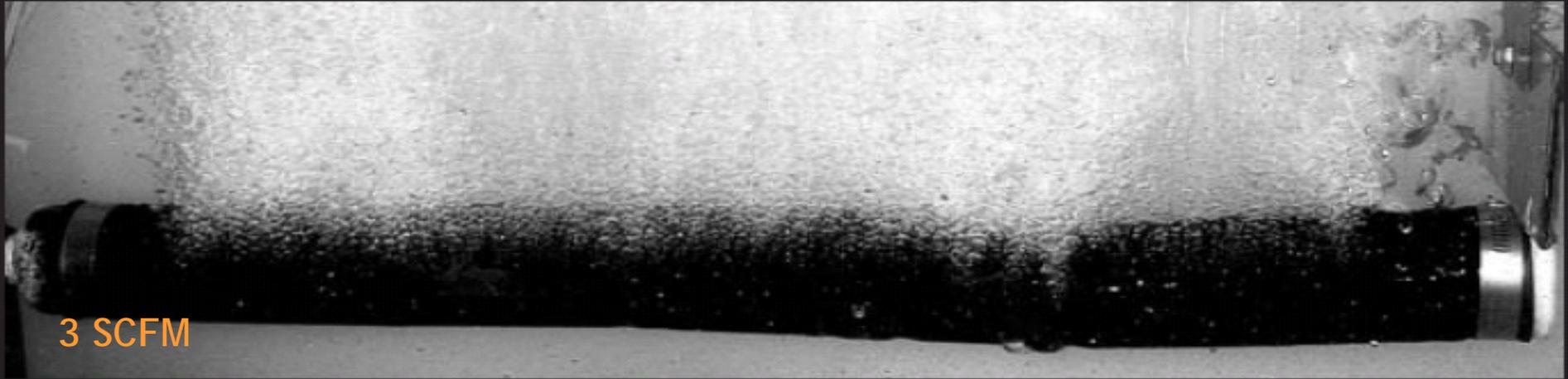


Minimum Pore Opening Threshold

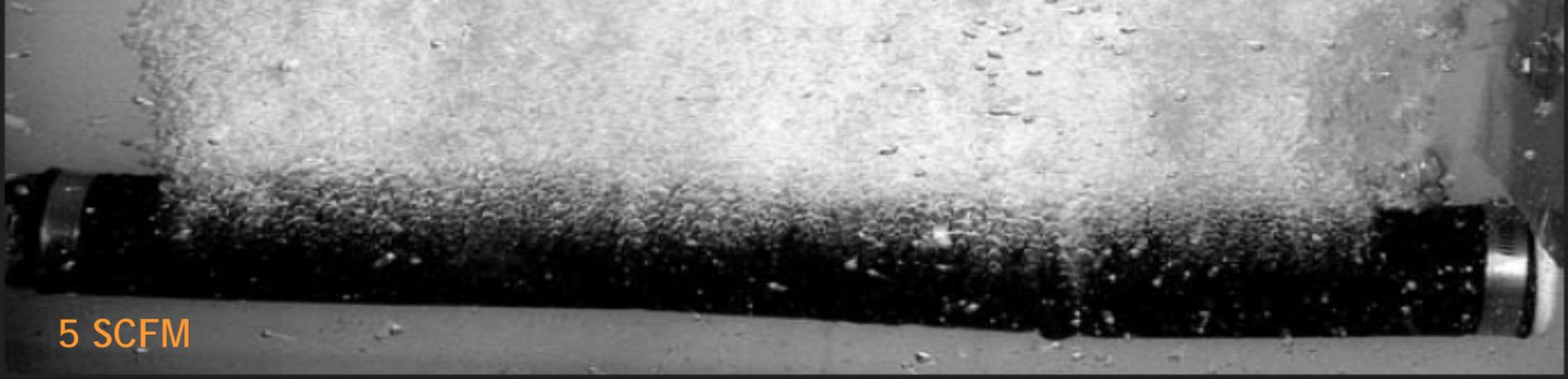
1 SCFM



3 SCFM



5 SCFM





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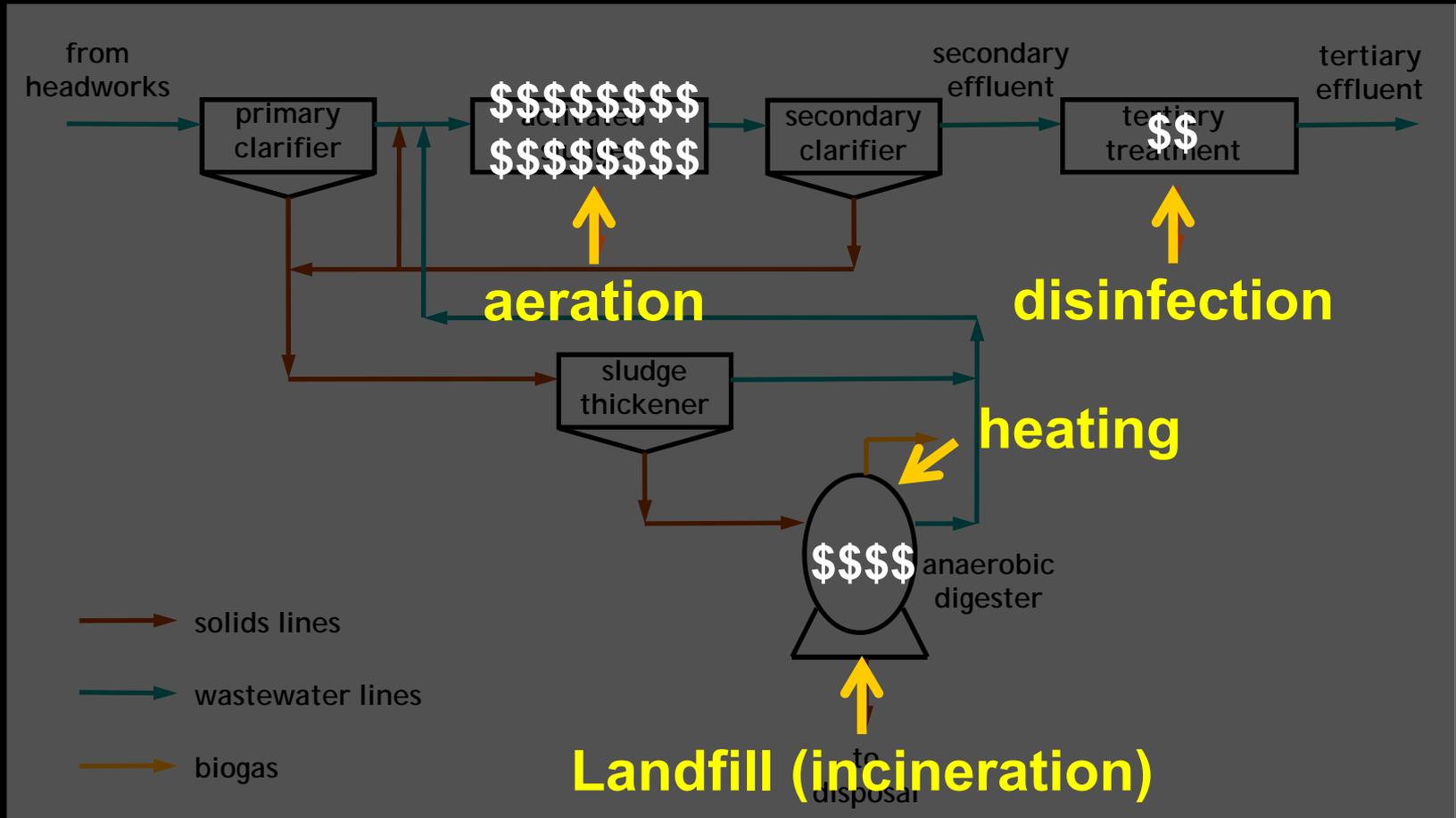
VI. AERATION MODELING AND ENERGY FOOTPRINT ANALYSIS

IN MY BACKYARD

- In CA, water conveyance is the largest energy consuming industry (~15%: 30,000 GWh)
- Water/Wastewater Treatment is second! (~6%)
- Wastewater Aeration ~ 45-75% of treatment energy

Data: CEC (2005); Rosso and Stenstrom (2005)

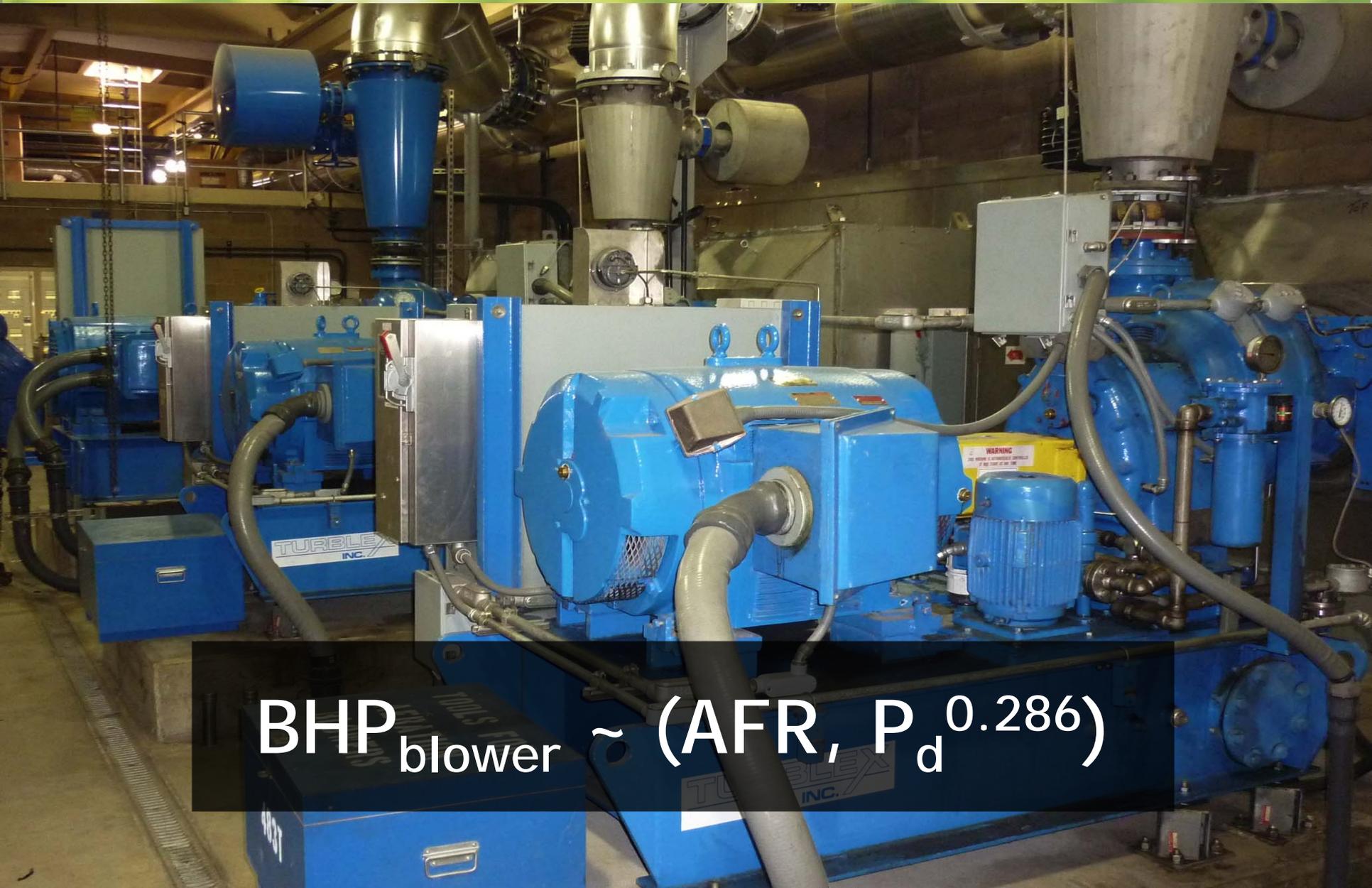
ENERGY FOOTPRINT



Aeration cost = 45-75% of plant energy (w/o influent/effluent pumping)

Rosso and Stenstrom (2005) *Wat. Res.* 39: 3773-3780

BLOWER POWER



$$\text{BHP}_{\text{blower}} \sim (\text{AFR}, P_d^{0.286})$$

AERATION & ENERGY FOOTPRINT

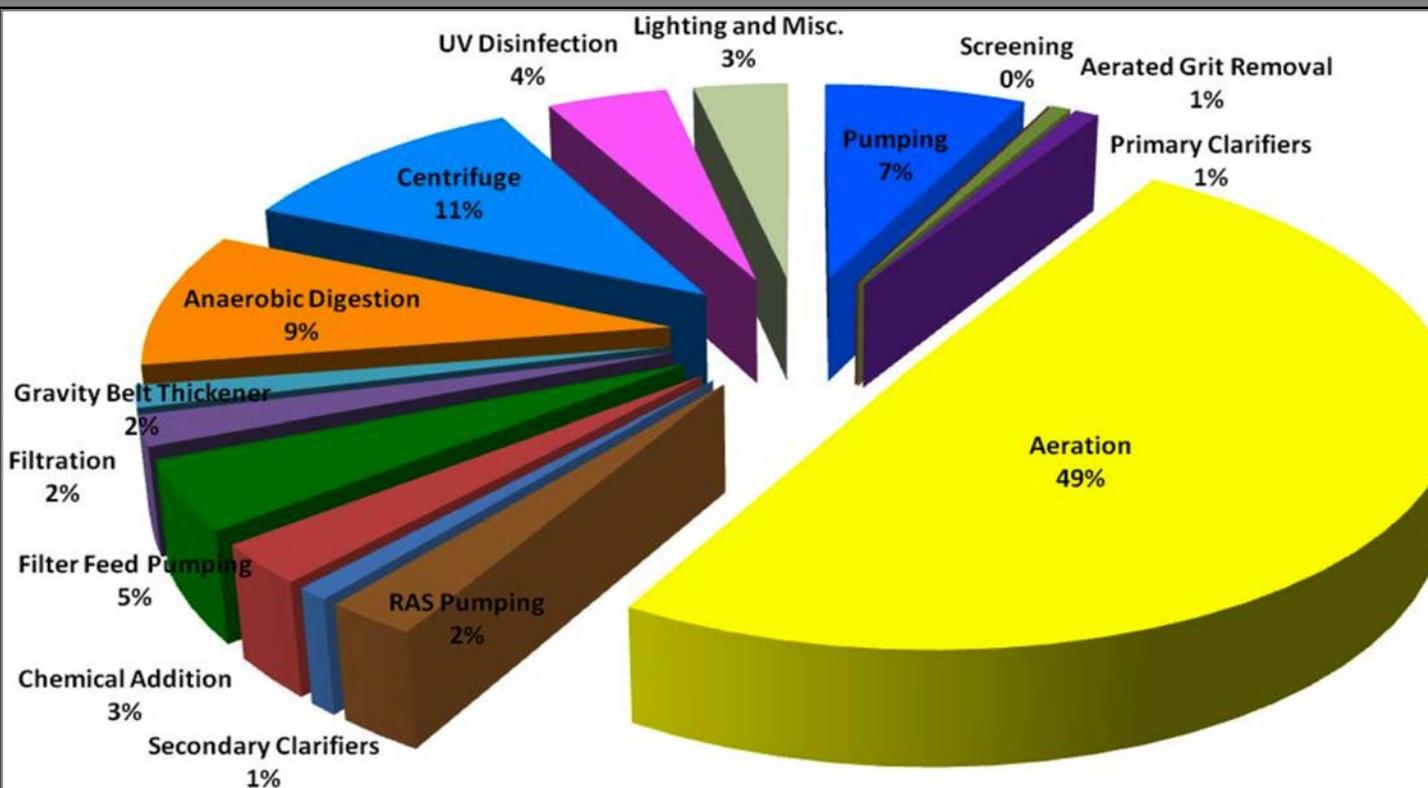
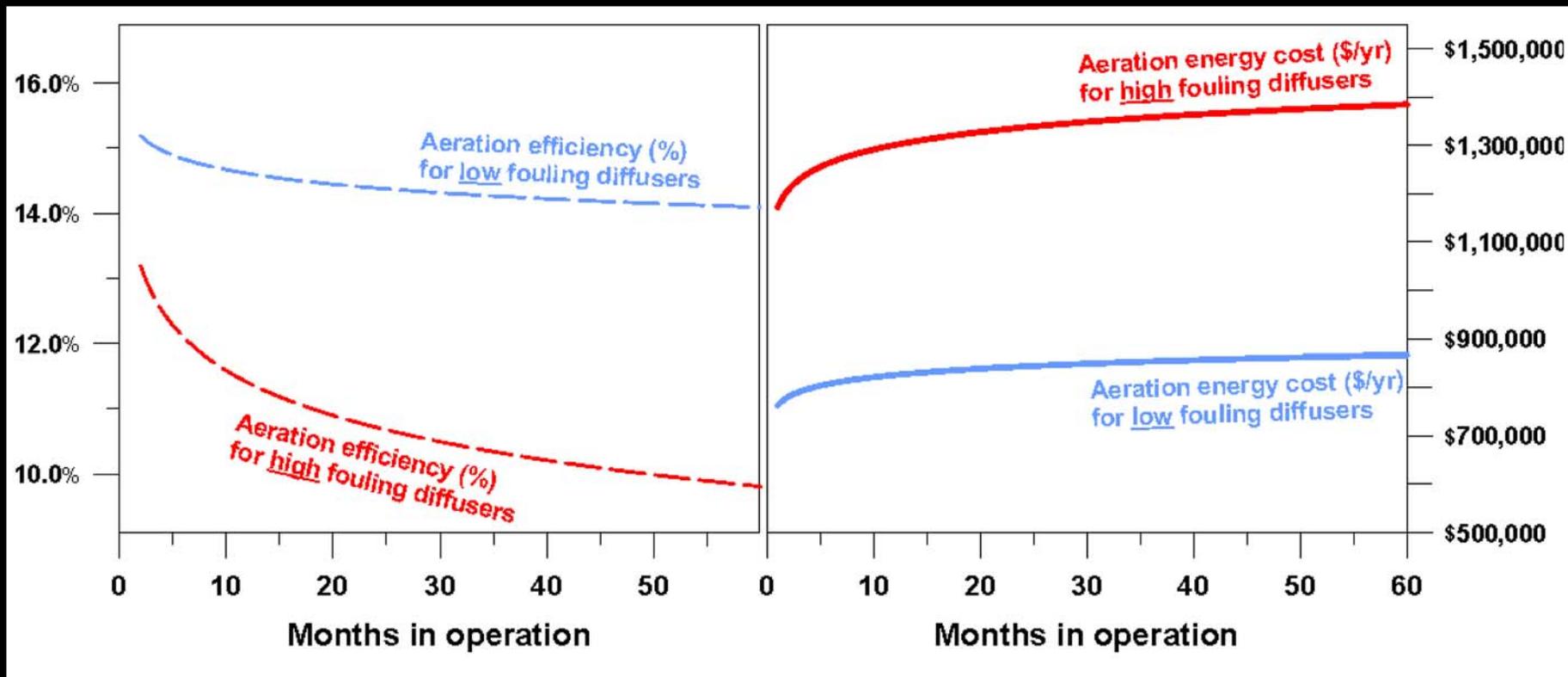


Figure 1. Estimated power usage for a typical 20MGD activated sludge facility performing wastewater treatment with nitrogen removal in the United States (MOP32, 2009).

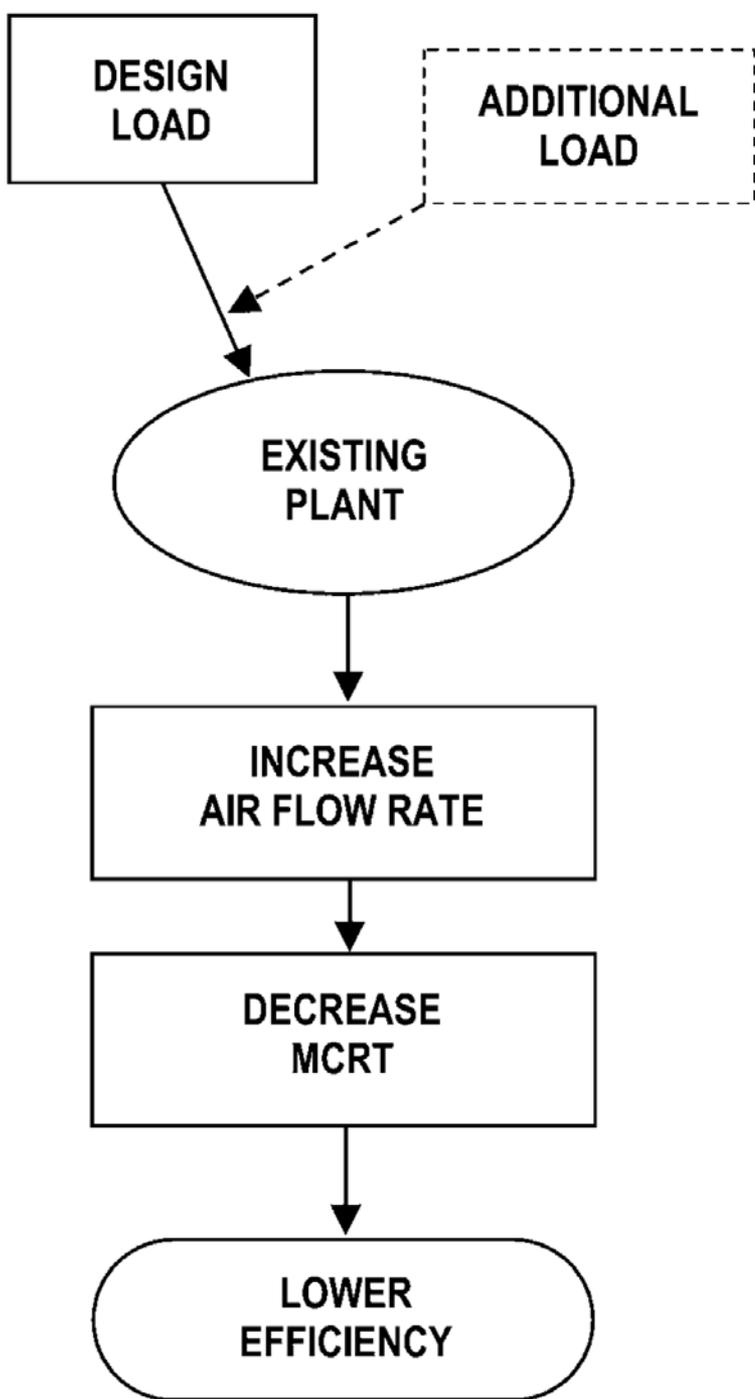
Aeration cost = 45-75% of plant energy (w/o influent/effluent pumping)

Rosso and Stenstrom (2005) *Wat. Res.* 39: 3773-3780

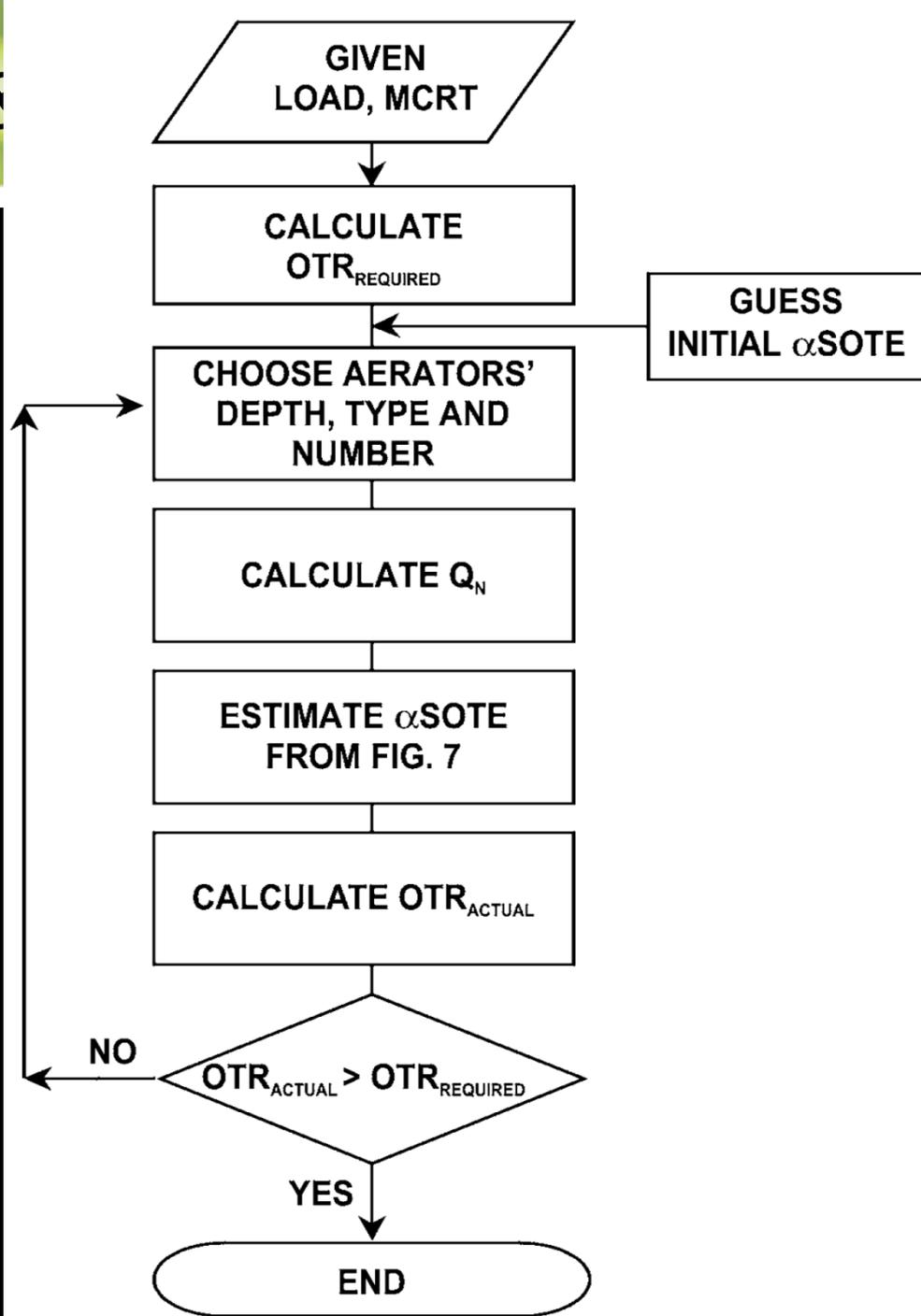
Process condition, \langle SOTE, and \$/yr



Aeration efficiency (%), oxygen transferred to the wastewater divided by the oxygen actually blown through the wastewater) and energy cost (\$/yr) estimation for US installations employing low and high fouling diffusers. The aeration energy cost here is estimated conservatively as the pure energy cost of blowing air (i.e., the additional maintenance required to run an inefficient system is not included). The difference between the initial values in the two graphs is due to differences in diffuser pressure drop.



8

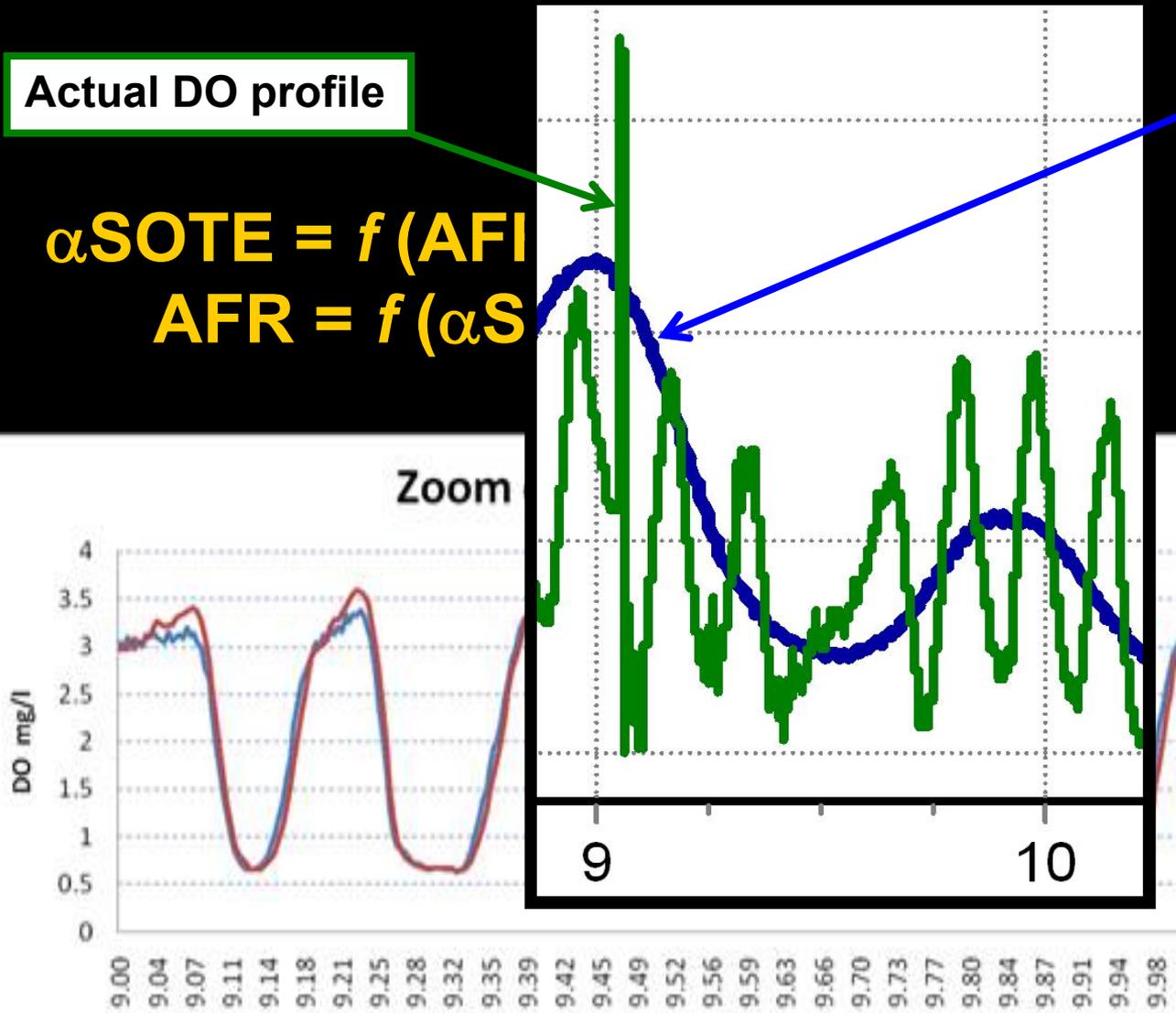


Static vs. dynamic aeration modeling

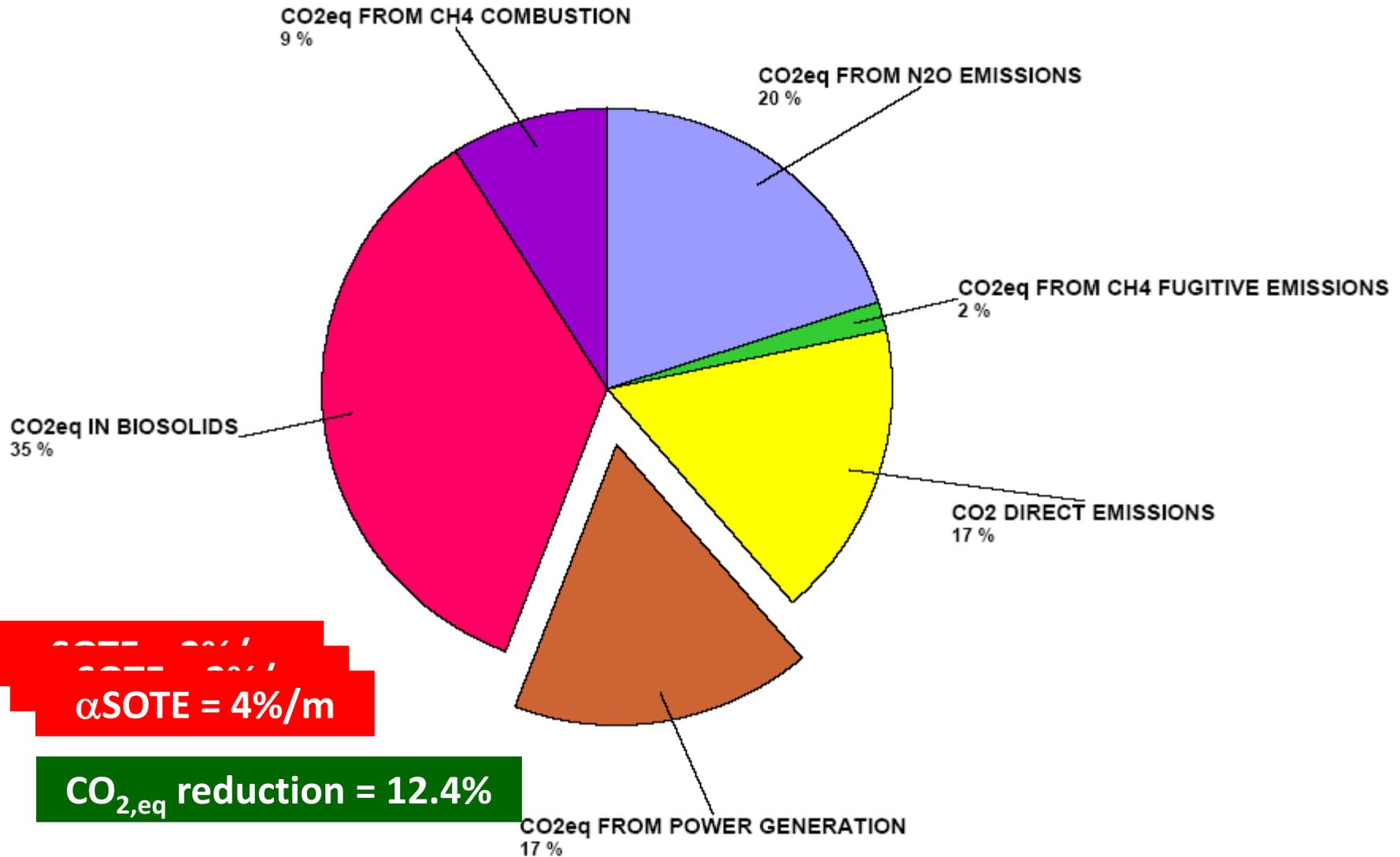
Actual DO profile

$$\alpha\text{SOTE} = f(\text{AFI})$$
$$\text{AFR} = f(\alpha\text{S})$$

DO profile modeled with constant αSOTE



Weight of aeration efficiency on process CFP

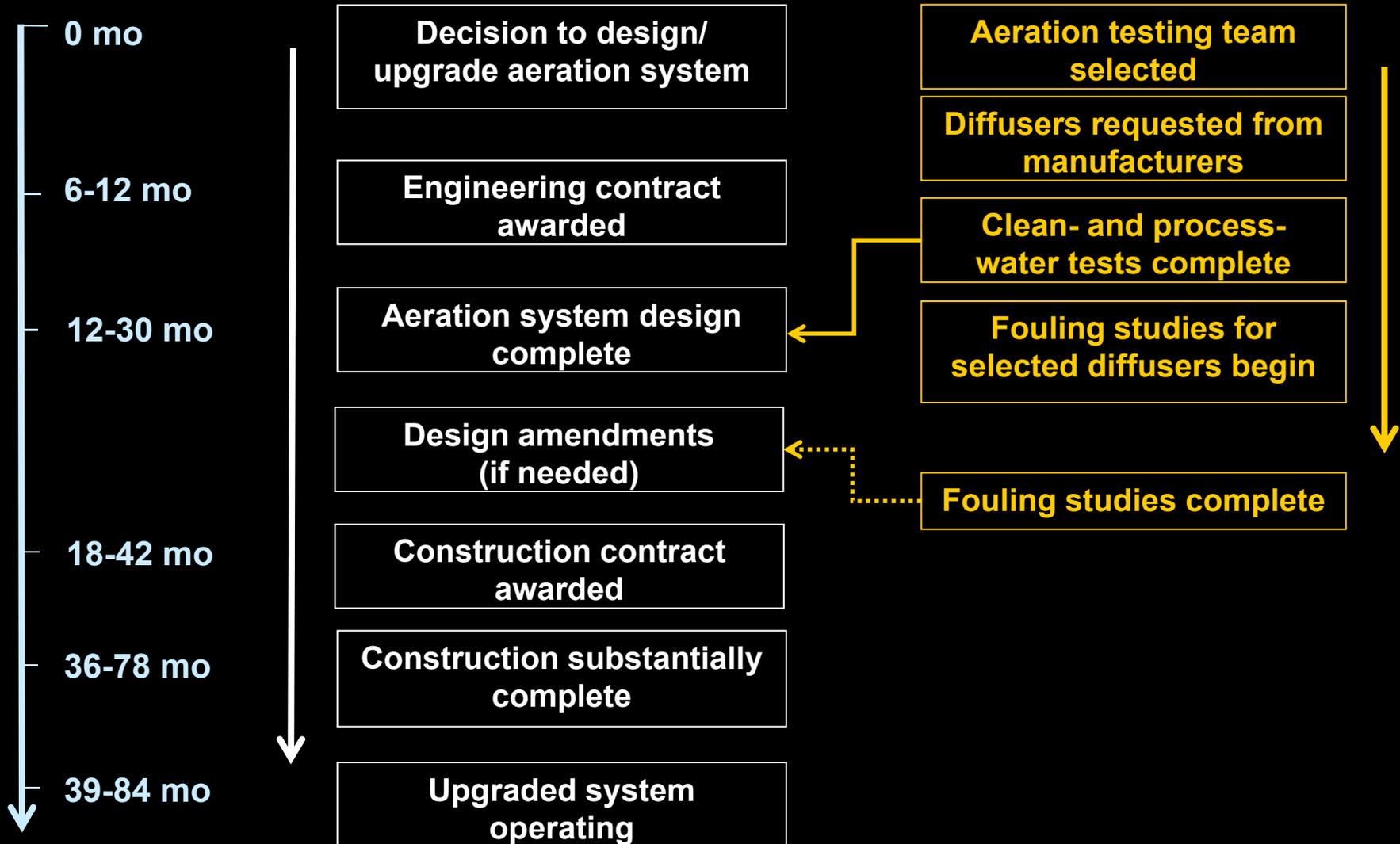


New design/upgrade paradigm

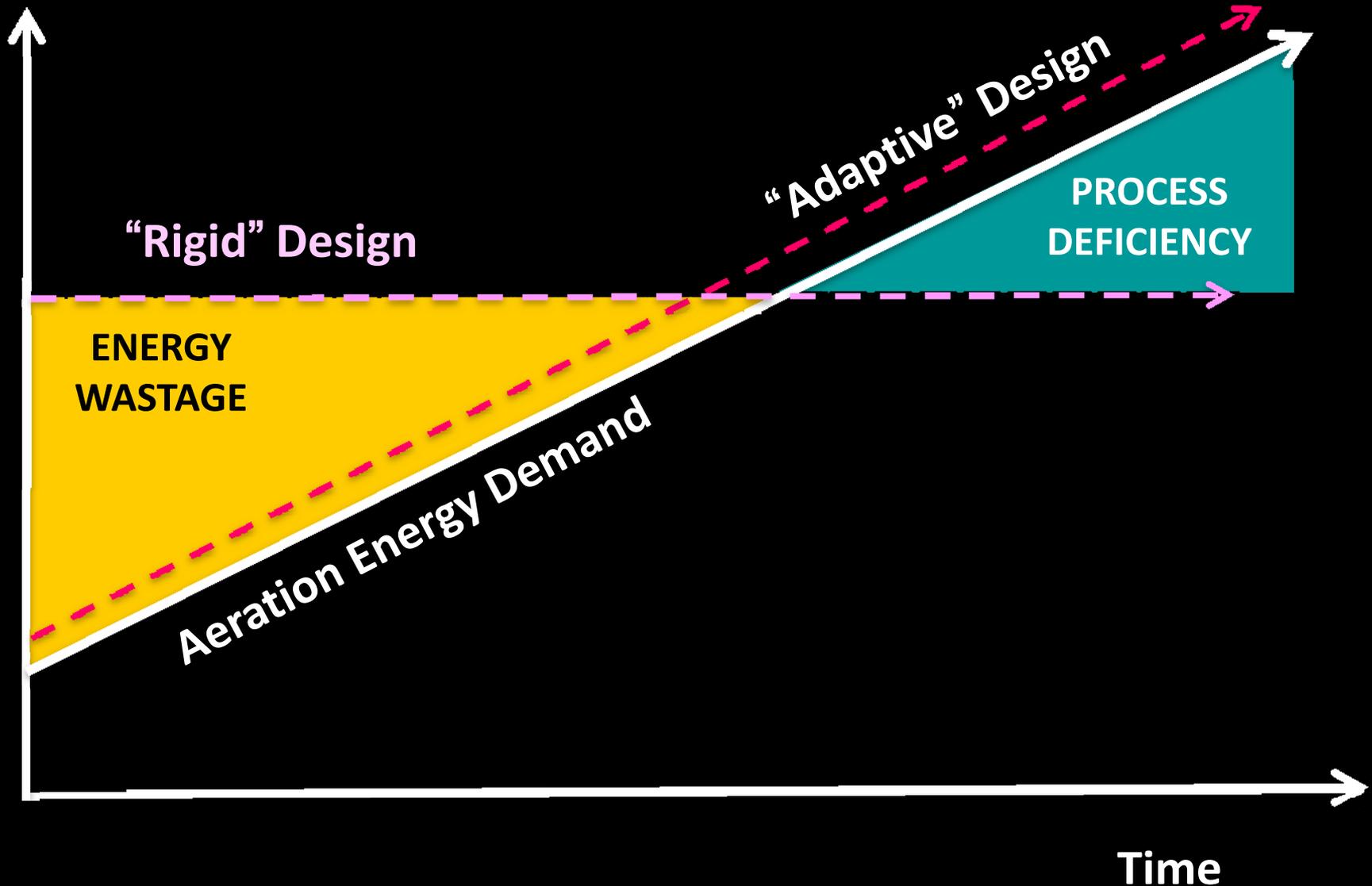
Time elapsed

Project timeline

Column testing steps



“Rigid” vs. “Flexible” Design



VII. CONCLUSIONS

CONCLUSIONS

- Contaminants accumulation depresses oxygen transfer and causes an increase in energy usage
- Aeration system and biological process layout influence oxygen transfer efficiency
- Real-time efficiency analyzers are available
- 24hr observations necessary for highest energy savings and for truly dynamic modeling
- Long-term studies quantify fouling effects and cleaning schedules
- Dynamic modeling allows the largest energy and carbon footprint minimization



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EPL

**ENVIRONMENTAL
PROCESS
LAB**

- Rosso et al (2005) *Water Environment Research* 77, 266-273
- Rosso and Stenstrom (2005) *Water Research* 39, 3773-3780
- Rosso and Stenstrom (2005) *Water Environ. Res.* 78, 810-815
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- Leu et al (2009) *Water Environment Research*, 81 2471-2481
- Kim et al (2009) *IEEE*

